

Research Article

Investigating the Performance of Puxin Model Anaerobic Digestion Reactor in a Tropical Country: Case of Togo

Maglwa Tcha-Thom^{1, 3, *} , Edem Komi Koledzi^{2, 3} , Gnon Baba² 

¹Department of Life and Earth Sciences, University of Kara, Kara, Togo

²Department of Chemistry, University of Lomé Lomé Togo

³Biomass and Bioenergy Technologies Laboratory (LT2B) & WASCAL, University of Lomé Lomé Togo

Abstract

The reaction environment of small-scale anaerobic digestion plants, is generally neglected and unmonitored, reducing their performance and face challenges in their widespread adoption. Thus, the objective of this work was to study the reaction environment and the structural optimization points of Puxin model anaerobic digestion reactors in mesophilic conditions under a tropical climate. Three 10 m³ Puxin model biodigesters were installed in series within a slaughterhouse for the anaerobic digestion of slaughterhouse wastes. Indicator parameters of stability (pH, redox potential and temperature) and performance (biogas flow rate, biogas quality) were monitored on-site, and organic and mineral loads (chemical oxygen demand, Total Kjeldhal nitrogen, conductivity) and inhibitors (Volatile fatty acids, total alkalinity) were assessed in the liquid fraction. The stability parameters pH and Eh, reached their optimal values while the digestion temperature settled at 31 ± 2 °C lower than the optimum value of 35 ± 2 °C. The temperature in the puxin model reactor was feedstock dependent and was not affected by external temperature of tropical climate. The methane content of the biogas varied between 48 and 65%. The biogas flow rate fluctuated between 0 to more than 33 L_{biogas}.min⁻¹ equivalent to a pressure of 3 to 8 kPa, satisfactory values for domestic use. The inhibitory parameters were within their optimal range for anaerobic digestion.

Keywords

Puxin Biodigester, Construction, Structural Optimization, Functional Monitoring, Biogas Quality, Biogas Flow Rate, Slaughterhouse Wastes

1. Introduction

Anaerobic digestion, a biochemical technological process for the treatment of organic wastes such as animal manures, industrial effluents and agricultural residues, has received increasing attention in recent years and highly used for animal wastes anaerobic digestion. The process involves degradation

and stabilization of complex organic matter by microorganisms leading to the production of biogas and digestate including solid and liquid as a consequence of energy and fertilizers recovery respectively. The process distinguishes small-scale digesters, medium scale and industrial scale digesters. Small-scale digesters or domestic/residential digesters have a power

*Correspondence: Maglwa Tcha-Thom (tchathommaglwa@yahoo.com)

Received: 3 August 2026; **Accepted:** 21 August 2026; **Published:** 15 September 2026



Copyright: © The Author(s), 2026. Published by Science Publishing Group. This is an **Open Access** article, distributed under the terms of the Creative Commons Attribution 4.0 License (<http://creativecommons.org/licenses/by/4.0/>), which permits unrestricted use, distribution and reproduction in any medium, provided the original work is properly cited.

supply capacity less than 25 kW or a volume going from 3 to 30 m³ and are meant to supply energy for cooking, lighting or sanitation in rural residential areas. Medium scale or commercial digesters with a capacity between 25 and 250 kW or a volume going from 50 to 500 m³ and meant for heating or electricity generation and large-scale installations with a capacity greater than 250 kW or a volume of more than 500 m³ [1]. They process the organic substrates into digestate and biogas which is composed in majority by 40 to 70% of methane and 30 to 60% of carbon dioxide [2-6]. Depending on the technology, they can be implemented in various types of climates and consists of thermophilic (45 - 60 °C), mesophilic (20 - 45 °C), or psychrophilic (< 20 °C) digestion [7]. Available small-scale biodigesters consist of fixed dome, floating dome, bag digester, portable digester. But the most developed domestic biodigester technology in Africa is the fixed-dome digester running in mesophilic conditions [7, 8]. The main characteristics of most of these small-scale biodigesters models are their small size, heating and substrate mixing are very limited and operate in wet-conditions. Structurally, they are composed of the substrate feeding/extraction pits, the digester core, and the biogas storage unit, usually integrated into the digester. The volumetric production of the different domestic digesters ranges from 0.1 to 0.4 m³ biogas/m³ digester/day for fixed dome digesters (Chinese, Camartec), 0.4 to 0.8 m³ biogas/m³ digester/day for floating dome digesters (Indian Gobbar, Puxin), and 0.25 to 0.6 m³ biogas/m³ digester/day for bag digesters and plug flow digesters. Among these biodigesters, the Puxin digester model has a high and stable pressure production of biogas and used for livestock effluents, human excrement, wastewater, straw, and food waste. The model was developed by the Shenzhen company, established in 2001 in China. It consists of domestic-sized (6 and 10 m³) and semi-industrial-sized (> 50 m³) units characterized by cylindrical, vertical reactors in a single cross-section, generally constructed of concrete using pre-designed molds. The integration of this model of biodigester in Togo's republic need to analyze its integration. Thus, the objective of this work is to study the reaction environment of Puxin model anaerobic digestion reactors in mesophilic conditions under a tropical climate. Four

biodigesters were therefore implemented in a sheep and goats slaughterhouses for the anaerobic digestion of the produced wastes. The process of implementation was analyzed and stability, inhibitors, organic and mineral load were monitored to ensure the performance of the reactor.

2. Materials and Methods

2.1. Area of Construction

The site for the implementation of the biodigesters was chosen taking into account the constant and sufficient availability of biodegradable substrates, the energy needs to be met, and the availability and strong motivation of the beneficiary to ensure the operation of the installation. The safety distance between trees and the installation site is greater than 50 m, eliminating any suspicion of weakening or collapse of the biodigesters due to established root development. Furthermore, the piezometric level, the avoidance of construction in flood zones, the 30 m safety distance from wells and surface water, and the downstream location of the biodigesters in relation to groundwater flow were not considered critical factors during the installation process. Thus, three 10 m³ Puxin digesters were installed in Agoe sheep and goat slaughterhouse.

2.2. Design and Construction

The system design considered two major parameters: retention time (RT) and daily slaughterhouse waste production, based on a digester installation with a capacity of 10 m³. Retention time is determined by the digestion temperature (25-30 °C) and the substrate dry matter content (16% of dry matter). The daily organic load (ORL) was determined and the number of biodigester to build was estimated to 02. Two biodigesters of 10 m³ were therefore built for solid wastes anaerobic digestion, with an additional biodigester to ensure the maturation of the liquid digestate (Table 1).

Table 1. Calculation method for sizing biodigesters.

Retention time: RT (jr)	Daily waste production: Pj (kg MB)	ORL = Biodigester volume/RT	Number of digester (N) N=Pj/ORL
RT= 66	Pj = 208	Volume of biodigester = 10 m ³ = 10 000 dm ³ ORL = 10000/66 = 151 kg.day ⁻¹	N= Pj/ORL = 1,4≈2

The installation is characterized by the site preparation phase followed by construction. Site preparation consisted of precisely locating and marking out the construction area for the biodigesters. Excavation of a pit of 3 meters depths and 4

meters in diameter was realized. The subsoil was prepared by laying a 10 cm thick layer of sand to prevent any potential cracks on the back face of the digester bases.

The biodigesters were constructed by assembling the molds

(body, arches, collar, pins) in the pre-existing pit as designed by Puxin company (Figure 1). Concrete, made from a mixture of 50 kg of cement, 60 L of sand, 130 L of gravel, and 25 L of water, was poured into the base on which the mold assembly rested and between the plates. The extraction and feeding pits are constructed using concrete blocks through which 1.25 m

long of 160 mm Polyvinyl chloride (PVC) pipes pass, forming the channel through which the substrates were introduced. The 160 mm PVC pipes was inclined at 45° and their lower edge was located 50 cm from the base of the digester. The bell was then placed in position, and protective concrete slabs protect it from potential external hazards or from being blown off its base due to the pressure generated by the biogas.

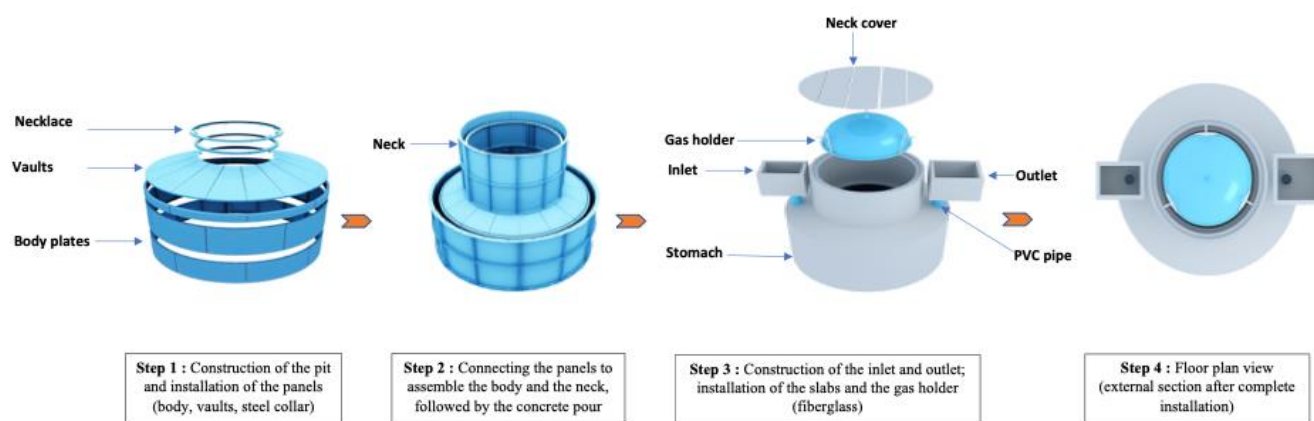


Figure 1. Process of Puxin biodigester construction.

Polyethylene pipes ($d = 9$ mm) connect the bell to the source of biogas consumption. The pipes were equipped with manometers with a maximum pressure of 16 kPa, which helped to detect leaks following untimely drops in pressure. The pressure gauges were followed by a water trap with a volume of 0.5 L to retain the water produced during the cooling of the biogas preventing any obstruction of the passage of the biogas. Sulfur filters containing iron filings purify biogas from sulfur. Water and air tightness tests were carried out to respectively check the tightness of the digester and the piping/bell. Water-tightness tests were carried out by filling water into the digester and measuring losses after 24 hours, 48 hours, 72 hours and 96 hours. Airtightness tests were carried out using biogas and water. Biogas is filled through all the piping which is then immersed in water. Leaks are identified by the formation of air bubbles.

2.3. Solid Substrates Characterization and Reactor Start-Up

A 10 kg mass of slaughterhouse waste was sampled and then transferred to the laboratory at room temperature (25 °C). The samples were characterized in terms of pH, dry matter, and volatile matter in triplicate. The pH was determined according to standard NF ISO 10390 (1994) using an Inolab-IDS-WTW Multi 9430 pH meter with a Sentix 980 electrode. The dry matter content was determined according to standard NF ISO 11465 (1994) using a Firlabo oven by drying at 105 ± 2 °C. The organic matter content was evaluated by loss on ignition at 550 °C for 4 hours using the SNOL 4011200 oven.

The start-up of biodigesters was subdivided into three main stages, including the determination of the dry matter and volatile matter content of the substrates; the introduction of 10 m³ of water in which 1 m³ of inoculum, representing 1/10 of the biodigester's volume; and the monitoring and observation of the initial biogas production from the inoculum, which serves to initiate daily feeding.

The initial organic load was estimated at 16.5 kg_{DM}/m³. The daily feeding of the biodigesters with raw substrates fluctuated between 100 and 150 kg, corresponding to an average organic load of 2.1 kg_{DM}/m³. Slaughterhouse substrates were used in this study as both inoculum and digestion substrates because their high microbial load and readily biodegradable.

2.4. Physico-chemical Monitoring in the Reactor

The pH, the redox potential, and the conductivity within the biodigester were monitored using the PHT-027 multiparameter meter, with a pH probe (Ag/AgCl electrode), an ORP probe, and a conductivity probe. The pH meter was calibrated using three buffer solutions: 4.01, 6.86, and 9.18. The accuracy is 0.1 pH unit for the pH probe and 0.1% for the ORP probe. The temperature within the biodigester was determined using the Vici TM803 thermometer probe. The temperature measurement range was -50 °C to +70 °C with an accuracy of ± 1 °C. The pH, redox potential, and conductivity within the biodigester were measured through the extraction and feed pits, and at various depths, including 1 m, 2 m, and 2.75 m allowing the

calculation of the daily average values.

2.5. Evaluation of Organic Load and Inhibition Parameters

Chemical Oxygen Demand (COD) and Biological Oxygen Demand (BOD₅) were measured by potassium dichromate digestion and respirometry using the SELECTA Digest Block 6 and the Aqua-Lytic AL606 BOD system, respectively. Total Kjeldhal Nitrogen (TKN) was determined by mineralization with H₂SO₄ in the presence of a catalyst (K₂SO₄ + Se) using the SELECTA Digest Block 6, followed by distillation with the Kjeltec Tecator 2200 distiller and titration with 0.1M NaOH. Volatile fatty acids (VFA) and total alkalimetry (TAC) content were determined by titration with H₂SO₄ and NaOH (1N and 0.1N).

2.6. Evaluation of Biogas Flow Rate, and Quality

The biogas flow rate was measured using the Argon type Gas Flow Meter Tester from two different biogas outlets, first

at the outlet of the biodigester (during 30 days) and second at the outlet of the biogas storage tank.

The methane content was determined by sampling the biogas using a syringe and measuring it volumetrically by moving the liquid. The first liquid is a solution of distilled water acidified to pH 2 using HCl and measures the total volume of biogas and the second is a KOH solution of pH 11 and measures the volume of methane in the biogas.

3. Results and Discussion

3.1. Biodigesters Construction and Leak Test Realization

The construction of the biodigester, the pipe installation and 24 hours system verification for leaks were completed in 5 days with a workforce of four and a concrete mixer including. Indian Gobarr, and Chinese biodigesters models require significantly longer construction times, ranging from 10 to 20 days, with a similar workforce. The quantities of materials used for the treatment of the subsoil and the construction are indicated Table 2.

Table 2. Volumes of materials used for the construction of a Puxin biodigester 10 m³.

Materials	Unit	Quantity per digester
Cement	kg	1600-1800
Sand	m ³	4-4,5
Gravel	m ³	6
Iron bar of 6/8, length 12m	unit	4-5
Pipes PVC 160	m	1,25 x 2
Bricks	unit	100
Wire coil	unit	01
Plaster	unit	01
Used oil for mol lubrication	L	3

Water tightness testing of the digesters revealed an average water loss of 1.2 cm (0.3 m³), 1.8 cm (0.5 m³), and 1.2 cm (0.3 m³) after 24 hours respectively for Digester 1, Digester 2 and Digester 3. These losses were attributed to absorption by the concrete and evaporation. This water loss stabilized at 0.5 cm after 72, 96, and 120 hours, indicating that the systems are watertight. The low water losses was attributed to evaporation. The water tightness testing technique was similar to that defined by [9], who suggested gradually filling the digester with water and assessing the losses over 2 to 4 days. Lacour [10] emphasizes that leak tests are recommended for three main

reasons: i) the eradication of groundwater pollution, ii) the reduction of water losses from digesters, and iii) the reduction of gas leaks that hinder pressurization of the biodigester.

The gas leak test was performed on both the fiberglass chamber storing the biogas within the biodigester and the piping used to deliver the gas to the point of consumption. Excess water was added to the upper limit of the chamber. The absence of air bubbles indicated a perfect seal on the chamber. For the piping, the biogas flows under pressure through the piping. Immersing the piping in water confirmed the absence of leaks due to the lack of air bubbles. The technique devel-

oped by Chanakya [9] for verifying gas tightness requires injecting air into the system at a differential pressure of 50 mbar

and checking its stability after 2 hours. The design of the complete installation is shown in Figure 2.

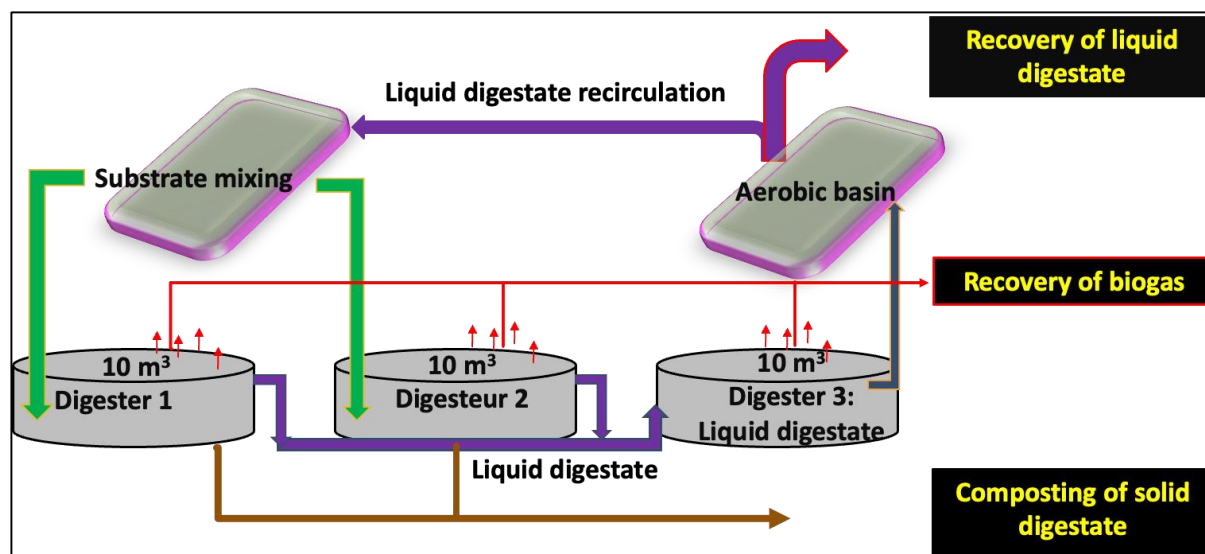


Figure 2. Design of the installation.

3.2. Inoculation of the Biodigester by the Substrates

Substrates from the rumen of slaughtered small ruminants were used simultaneously as inoculum and subsequently as substrates for methanation, given their high concentration of bacterial flora and known high buffering capacity. The volatile matter of the inoculum was $98 \pm 2\%_{DM}$ and the dry matter was $17 \pm 3\%_{DM}$ [11]. The pH (7.1 ± 0.5) was suitable for anaerobic digestion, and the mineral load, reflected by the conductivity, is approximately $3317 \pm 210 \mu S \cdot cm^{-1}$.

Compared to conventional digesters characterized by two- or three-stage inoculation [9], the inoculation of the digesters in this study using slaughterhouse wastes was carried out in a single stage by introducing $1 m^3$ of inoculum into a liquid phase of $10 m^3$ of water. This unique inoculation method, used in Puxin technology, eliminates any immediate inhibition and allows for gradual colonization of the digestion medium. Biogas production ($> 1 m^3$) was achieved in less than 12 hours. Flammability tests were positive, with a blue flame indicating effective methanogenic activity.

3.3. Studying Stability Parameters of the Biodigester in Situ

A sudden change in temperature can cause a functional imbalance in the microbial population [12]. Gerardi [13] recommends a fluctuation between 2 and 3 °C in temperature to ensure the stability of the process in mesophilic conditions. Temperature in the biodigester varied between 29 and 33 °C with an average of 31 ± 1 °C, a deficit of around 4 °C compared to the optimal temperature in mesophilic digestion which is 35 ±

2 °C (Figure 3). The external temperature varied between 28 and 40 °C during the experiment phase, therefore the temperature measured within the biodigester was not a function of the external temperature in mesophilic conditions and in tropical regions. In contrary, it should be a function of the intensity of degradation of the organic load and therefore of bacterial activity. This analysis was confirmed by Pincam *et al.*, [8] who showed that, feedstock composition significantly influenced anaerobic digestion sensitivity to temperature change, readily degradable feedstock displaying greater sensitivity to temperature changes. The low digestion temperatures within biodigesters compared to the optimal digestion temperature in mesophilic digestion could reduce the performance of anaerobic digestion with the consequence of a reduction in the level of degradation and the qualitative production of methane and a low level of sanitation of the digestates. The temperature variations reported within biodigesters in Togo are higher than those measured in Haïti which oscillate between 24 and 31 °C, with an average of 27.4 °C, and environmental temperature conditions varying between 4 and 13 °C [10] while in Senegal [14] reported a variation between 29.1 and 36.6 °C with an ambient temperature of 26.8 to 31.6 °C. Studies revealed that, the temperatures and the average daily biogas productions were higher for the steel biodigester ($1.5 \pm 0.12 m^3 \cdot day^{-1}$ at 36 ± 2 °C) than those produced from the PVC ($1.3 \pm 0.1 m^3 \cdot day^{-1}$ at 31 ± 1.5 °C) and concrete ($1.2 \pm 0.05 m^3 \cdot day^{-1}$ at 27 ± 2 °C) biodigesters. So, the low temperature of the studied biodigester compared to the optimal values appropriate anaerobic digestion may be influenced by its state, built with cement [15]. Therefore, the external temperature might have a very slight impact on the internal temperature of the reaction medium of the digesters.

The pH varied between 6.5 and 7.8 with an average of 7.1

± 0.3 , adequate range for optimal anaerobic digestion (Figure 3). The high pH values were measured on the side of the substrate extraction pit while the low values were obtained on the side of the feeding pit. Lacour [10] highlights changes in pH in biodigesters of between 6.3 and 8.7 on a plug flow biodigester and [13, 14] reported a fluctuation between 6.8 and 7.7 for Puxin model biodigester very closed to the results of this study. Optimal activity of methanogens is favored by a pH between 6.8 and 7.2 [14, 16].

The optimum range of ORP for CH₄ reducing bacteria is below -230 mV [17-19]. The redox potential quickly reached the optimum for anaerobic digestion within 10 h after feeding and then stabilized between -250 and -315 mV (Figure 3). Considering the convenience, economic factor and reliability of industrial biogas plants of chicken manure, an ORP higher than -540 mV is an indicator of inhibition while a severe inhibition occur for an ORP higher than -520 mV [20].

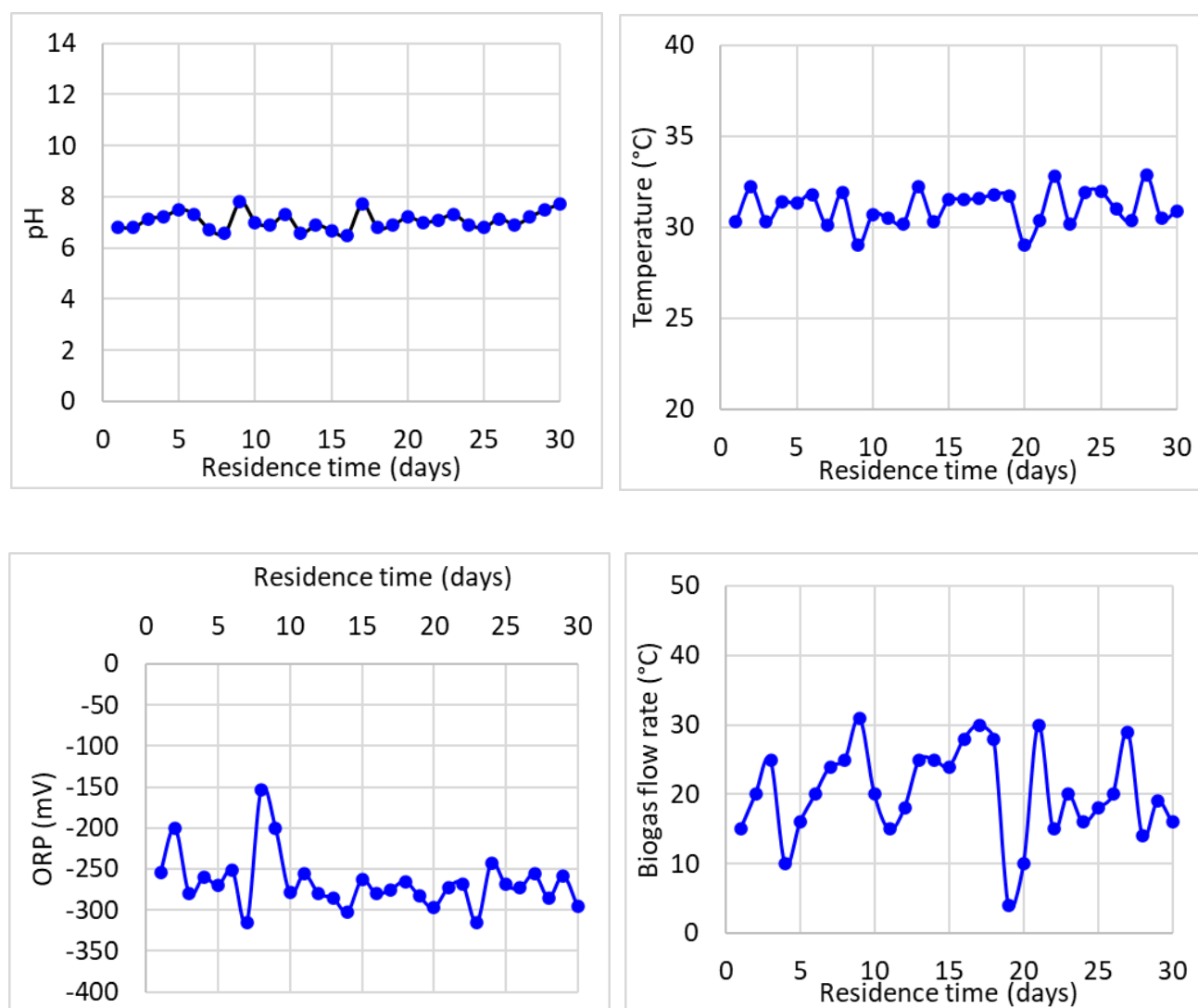


Figure 3. Physical and physico-chemical parameters evolution in biodigester.

3.4. Evaluation of the Organic Load and Inhibitors Parameters in Liquid Digestate

The mineral load, expressed as conductivity, the organic load, expressed as COD and VFAs, and the buffering capacity, characterized by TAC, were determined during the first two months of digester operation. These parameters were measured on the liquid phase, which is transferred daily from the

biodigesters receiving the solid substrates to the biodigester responsible for digesting the effluent. The mineral load increased from 500 to 5500 $\mu\text{S}\cdot\text{cm}^{-1}$. The TKN, COD, and VFAs changed from 50 to 400 $\text{mg}\cdot\text{L}^{-1}$, 250 to 4150 $\text{mg}\cdot\text{L}^{-1}$, and from 0.08 to 0.99 $\text{g}\cdot\text{L}^{-1}$, respectively. BOD₅ accounted for 54% to 89% of the COD, demonstrating high biodegradability of the liquid abattoir digestates. The TAC quickly reached the minimum desired value of 3 $\text{g}\cdot\text{L}^{-1}$. The VFA/TAC ratio varied between 0.09 and 0.4 and did not exceed the limit ratio of 0.8.

Some studies underlined TAC values slightly above 5 g.L⁻¹ ensuring a stabilization of the anaerobic digestion process, ammonium values in mesophilic conditions were under 1.5 g.L⁻¹ and soluble COD were approximately 900 mg.L⁻¹ at 37 °C up to 3500 mg.L⁻¹ at 53 °C [21].

3.5. Biodigester Performance: Flow Rate and Biogas Quality

The biogas flow rate generated by the biodigester varied between 3 and 33 L_{biogas}.min⁻¹ (Figure 3- biogas flow rate), the

equivalent of 3 to 8 kPa. Low flow rates and pressure are observed with biogas use. The average biogas flow rate was 20 L_{biogas}.min⁻¹. This pressure is similar to 0 to 6 kPa and 0.9 to 10.8 measured respectively by Tcha-Thom *et al.* [22] and Ebeya *et al.*, [14] on Puxin model biodigester. A 10 m³ digester in normal operation can reach a value of 12 kPa [14].

However, due to overproduction, transferring the biogas into 10 m³ tanks was considered. The biogas stored in these 10 m³ tanks exits at a flow rate of < 0.5 L_{biogas}.min⁻¹ hindering its use. Therefore, tests are being conducted to determine a suitable flow rate.

Table 3. Performance parameters of the biodigester.

	Pressure (kPa)	Biogas flow rate (L/min)	Methane content (%)
Biogas exiting directly from biodigester	3 - 8	0 - 33	
Biogas exiting from balloon	< 0.1	< 0.5	
Biogas exiting from balloon supporting load of 50 - 500 kg	0.5	< 0.5	45 - 64.5
Biogas exiting from balloon connected to booster pump	0 - 50	0 - 60	

Adding weights ranging from 50 to 500 kg to the biogas storage tank resulted in flow rate < 0.5 L_{biogas}.min⁻¹. This technique did not appear promising for optimal biogas utilization. Using the biogas directly from the biodigester provided better flow rate. The use of an electrically powered pressure regulator generated adjustable pressure, ranging from 0 to 60 L_{biogas}.min⁻¹, depending on the application. This flow rate allowed the use of generator for electricity production, and cooking.

The measured methane content ranges from 45% to 64.5%. On-site concentrations varying from 40 to 62.95% were reported on plug-flow digester in Ha fi and Puxin biodigester in Senegal [10, 14], while some authors reported very low concentrations of methane (29 to 47%) and high concentrations of 80 to 91% of fish wastes anaerobic digestion in mesophilic conditions [23, 24]. The methane percentages obtained by Faye [25] were 58.52% on cow dung, 62.95% on cashew apple and 61.3% in co-digestion of 50% on cashew pulp and 50% cow.

3.6. Structural Optimization: Automatic Water Drainage by Sloping the Pipes

During the operation of the biodigesters, the absence of biogas at the point of consumption was reported three times in six months. This was due to failure to adhere to the monthly drainage schedule for water droplets formed during gas cooling in the piping, preventing the biogas from reaching the point of consumption. Tests to drain the water from the piping determined that the emptying time was one hour by two people for three biodigesters. However, the operators found this

operation very tedious. Previously, the piping was horizontal and at the same level as the top of the tank. Raising the piping and placing it at an angle resolved the problem. This allows the water to return to the biodigester by gravity without external intervention, thus ensuring the regular presence of biogas at the point of consumption.

4. Conclusion

The objective of this work was to study the structural optimization points of the anaerobic digestion reactors of the Puxin model under a tropical climate and to analyze the reaction environment during mesophilic operation. The stability parameters, inhibitors, and organic and mineral loading were found to be within the acceptable digestion ranges for mesophilic digestion. The performance parameters were adequate for biogas production. Structural optimizations were tested and validated for the optimization of the Puxin biodigester. This study thus provides insight into the operating regime of the Puxin model in a tropical climate, facilitating its successful dissemination.

Abbreviations

RT	Retention Time
ORL	Daily Organic Load
PVC	Polyvinnyl Chloride
COD	Chemical Oxyxygen Demand
BOD5	Biological Oxygen Demand on Five Days

TKN	Total Kjeldhal Nitrogen
VFA	Volatile Fatty Acids
TAC	Total Alkalimetry

Acknowledgments

The authors are grateful to French Funds for the World Environment (FFEM)/UICN, European Union (EU), Suez Funds, French Agency for Development (AFD), La region Iles de France and Republic of Togo Government for supporting this research towards the construction of the Puxin biodigesters.

Author Contributions

Maglwa Tcha-Thom: Conceptualization, Data curation, Formal Analysis, Funding acquisition, Investigation, Methodology, Software, Visualization, Writing – review & editing

Edem Komi Koledzi: Data curation, Funding acquisition, Investigation, Project administration, Supervision, Validation, Writing – review & editing

Gnon Baba: Data curation, Funding acquisition, Investigation, Project administration, Supervision, Validation, Writing – review & editing

Data Availability Statement

The data supporting the outcome of this research work has been reported in this manuscript.

Conflicts of Interest

The authors declare no conflicts of interest.

References

- [1] Mutungwazi, A., Mukumba, P., Makaka, G. (2018). Biogas digester types installed in South Africa: A review. *Renewable and Sustainable Energy Reviews*; 81 (1): 172-180.
- [2] Bond, T, Templeton, M. R. (2011). History and future of domestic biogas plants in the developing world. *Energy Sustain Dev*; 15: 347–54. <http://dx.doi.org/10.1016/j.esd.2011.09.003>
- [3] Ononogbo, C. Nwufu, O. C., Nwaiwu C. F., Igbokwe, J. O. (2015). An innovative approach to construction and operation of biodigesters: a consideration of floating drum biogas plant. *TLEP International Journal of Mechanical Engineering Research*, 1 (3): 1 – 13.
- [4] Obileke, K., Mamphweli, S., Edson, L., Meyer, E. L., Makaka, G. and Nwabunwanne Nwokolo, N. (2020). Design and Fabrication of a Plastic Biogas Digester for the Production of Biogas from Cow Dung. *Hindawi Journal of Engineering*; pp1 -11.
- [5] Ojo, O. M., Babatola, J. O. (2021). Appraisal of Cumulative Volume of Biogas Produced from Water Hyacinth and Selected Animal Dungs Co-Digestion Mixes. *Journal of Civil Engineering and Urbanism*; 11 (5): 58-64.
- [6] Safley, Jr L. M., Westerman, P. W. (1992). Performance of a low temperature lagoon digester. *Bioresource Technology*; 41(2): 167–75.
- [7] Boers, W., Workneh, K., Esthete, G. (2008). National biogas programme - Ethiopia programme implementation document.
- [8] Pincam T., Liu T-Q., Short M., Guo B., Sadhukhan J., Bywater A. (2026). Challenging conventional temperature ranges in anaerobic digestion: intermediate (45 °C) as general optimum with feedstock-dependent performance differences from mesophilic (35 °C) and thermophilic (55 °C) conditions. *Bioresource technology*; 441: 133609.
- [9] Chanakya, H. N., Bhogle, S., Arun, R. S. (2005). Field experience with leaf litter-based biogas plants. *Energy for Sustainable Development*; 9(2), 49-62.
- [10] Lacour, J. (2012). Valorization of agricultural organic residues and associated wastes towards anaerobic biological treatments. University of Lyon; PhD Thesis; 218p.
- [11] Tcha-Thom, M., Baba, G., Feuillade-Cathalifaud, G., Pallier, V., Gnanvossou, D., Toko, M., Koledzi, E. K. (2018a). Comprehensive study of organic and inorganic compounds released by animal and pineapple fruits wastes. *Journal of Scientific and Engineering Research*; 5 (11): 32-42.
- [12] Kim, M. and Speece, R.E. (2002). Comparative process stability and efficiency of anaerobic digestion: mesophilic vs. thermophilic. *Water Research*; 36, 4369-4385. [https://doi.org/10.1016/S0043-1354\(02\)00147-1](https://doi.org/10.1016/S0043-1354(02)00147-1)
- [13] Gerardi, M.H. (2003). *The microbiology of anaerobic digesters, wastewater microbiology series* Hoboken, New Jersey: John Wiley & Sons, Inc.
- [14] Ebeya, C., C., Mahmoud, M., Sidibba, A., Yetilmezsoy, K., Kiyani, E., Kane, C., S., E., Bilal, B., Jedou, E., Youm, I., Ndongo, M. (2022). Influence of the construction materials properties of the biodigester on the biogas production and electricity generated by the slaughterhouse waste. *International Journal of Design & Nature and Ecodynamics*; 17 (4), 513-520.
- [15] Mansaly, J.B., Diouf, D., Piriou, B., Ndiaye, D. and Maïga, A.S. (2021) Study of the limit of the technological transition in the field of methanisation in Senegal (from Laboratory Scale to in-Situ Bi-odigester). *Journal of Sustainable Bioenergy Systems*; 11, 215-226. <https://doi.org/10.4236/jsbs.2021.114014>
- [16] Dana, R. (2010). Macro-Scale biogas production: A beginners guide. The national sustainable agriculture information service, ATTRA. <https://www.ncat.org/publication/micro-scale-biogas-production-a-beginners-guide/>
- [17] Hungate, R.E. (1969). Chapter IV a roll tube method for cultivation of strict anaerobes. In: Norris, J.R., Ribbons, D.W. (Eds.), *Methods in Microbiology*, Part B, Academic Press; 3: 117–132.

- [18] Vongvichiankul, C., Deebao, J., Khongnakorn, W. (2017). Relationship between pH, oxidation reduction potential and biogas production in mesophilic screw anaerobic digester. *Energy Procedia*; 138: 877-882.
- [19] Sukphun, P., Sittijunda, S., Reungsang, A., Atta-Obeng, E. (2021). Volatile fatty acid production from organic waste with the emphasis on membrane-based recovery. *Fermentation*; 7, 159.
- [20] Ao, T., Chen, L., Zhou, P., Lui, X., Li, D. (2021). The role of oxidation-reduction potential as an early warning indicator, and a microbial instability mechanism in a pilot-scale anaerobic digestion of chicken manure. *Rewable Energy*; 179: 223- 232.
- [21] Steiniger, B., Hupfauf, S., Insam, H., Schaum, C. (2023). Exploring anaerobic digestion from mesophilic to thermophilic temperatures—operational and microbial aspects. *Fermentation*; 9(9): 798; <https://doi.org/10.3390/fermentation9090798>
- [22] Tcha-Thom, M., Baba, G., Koledzi, K. E. (2018b). Waste recovery into biogas: promotion and suitability of bio-digesters in industrial units. *Technological Innovation and Management for Sustainable Development (For Greener, Safer and Smarter World)*; Gwalior, India. pp. 376-386.
- [23] Fall, M. (2018). Physicochemical characterization and energy recovery of solid waste in the Dakar region. Doctoral thesis, Cheikh Anta Diop University of Dakar.
- [24] Kebe, N.N., Fall, P.A., Ndiaye, D. and Diouf, D. (2019). Residues of the transformation of halieutics products: an alternative substrate for energy valorization of wastes by methanisation for a local sustainable development (preliminary results). *African Journal of Environmental Science and Technology*; 13, 291-295. <https://doi.org/10.5897/AJEST2018.2549>
- [25] Faye, O.K., Ndiaye, L.G., Sarr, B. (2020). Comparative Study of Anaerobic Digestion Between Cashew Apple Pulp, Cow Dung and Their Codigestion. *Soaphys Journal of Physics* 2(2630-0958): 1.

Biography



Maglwa Tcha-Thom is currently an Assistant-Professor in University of Kara (Togo), department of life and earth sciences. He holds a mixed PhD from the Universities of Limoges (France) and Lomé (Togo) in Water, Soil and Environment.

The area of expertise includes wastes and wastewater valorization into biogas and compost, environmental impact assessment, water potabilization and soil amendment. Maglwa thesis activities in the recovery of slaughterhouse waste into biogas allowed the NGO ENPRO to be the winner of the second edition of the Climate Initiatives Trophies held in Bonn in margin of COP 23. In 2017, he won the inter-university award on “Climate Variability”, Ethiopia. He regularly participates in the development and execution of projects and feasibility studies across Africa and capacity building on questions of strategic planning of the public waste service including composting, biogas production, leachate treatment, sustainability of operators and development of entrepreneurial strategies.

Research Field

Maglwa Tcha-Thom: Biomass to biogas and compost, Greenhouse gases, Wastewater treatment, Water potabilization, Environmental impact assessment, applied chemistry, Soil amendment

Edem Komi Koledzi: Chemistry, Biomass to biogas and compost, Greenhouse gases

Gnon Baba: Organic chemistry, Wastes management