

Copper (II) Ions Biosorption from Aqueous Solution Using Modified Moringa Oleifera Leaves (MMOL)

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Abstract: The present research work demonstrated the ability of MMOL in removing Copper (II) ions from an aqueous solution. The modified (MMOL) and unmodified moringaoleifera (UMOL) was characterized based on PZC and surface area. Isotherm experiments were conducted and the data obtained were fitted to Langmuir and Freundlich isotherm equations. The Freundlich equation gave the best description of the sorption process and the maximum saturated monolayer sorption capacity of the MMOL for CU (II) ions was 78.45 mg g⁻¹. The kinetics of the sorption process was studied by varying the initial CU (II) ions concentrations and the result obtained was analyzed by using pseudo-first-order and pseudo-second-order kinetic models. The pseudo second-order kinetic model was found to fit the experimental data for the entire sorption period with high coefficient of determination (r²). The effects of MMOL dose were studied using batch sorption system. The linear form of the Langmuir equation was used to analyze the data obtained when the sorbent dosage was optimized by method of continuous variation. The results obtained showed that the equilibrium monolayer sorption capacity, q_m, of the MMOL for CU (II) ions decreased (78.45 - 38.66 mg g⁻¹) with an increase in sorbent dosage. The result obtained from pH optimization showed that CU(II) ions removal increases with increase in CU(II) ions solution pH.

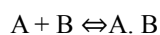
Keywords: Biosorption, Kinetics, Modified Moringaoleifera Leaves, Pseudo First Order, Pseudo Second Order

1. Introduction

Water pollution containing heavy metal ions such as chromium, cadmium, copper, lead, nickel, mercury and zinc from industrial and domestic wastes is becoming one of the most serious environmental problems worldwide [1]. Because of the low concentration of heavy metals in various resources it can be more harmful to the environment and adversely affecting the human health. The remedy of heavy metals is so significant because of the continuance in the environment. Industrial wastewater treatment covers the mechanisms and processes used to treat wastewater that is produced as a by-product of industrial or commercial activities. After treatment, the treated industrial wastewater (or effluent) may be reused or released to a sanitary sewer or to a surface water in the environment. Most industries

produce some wastewater although recent trends in the developed world have been to minimize such production or recycle such wastewater within the production process. However, many industries remain dependent on processes that produce wastewaters. Copper pollution generally arises from copper mining and smelting, brass manufacturing, electroplating industries and excessive use of Cu-based agrochemicals. In fact, copper is essential to human life and health, but like all other heavy metals, it is potentially toxic at high concentrations. The excessive amounts of Cu (II) in fresh water resources and aquatic ecosystem damage the osmoregulatory mechanism of the freshwater animals and cause mutagenesis in humans [2]. Large quantities of copper are released to the environment by discarding industrial waste without further treatment [3]. According to World Health Organization (WHO) the permissible limit of Cu (II) in water is 1.5 mg/l [2]. The most commonly used methods

for the removal of metal ions from industrial effluents include: chemical precipitation, solvent extraction, oxidation, reduction, dialysis/electrodialysis, electrolytic extraction, reverse osmosis, ion-exchange, evaporation, cementation, dilution, adsorption, filtration, flotation, air stripping, steam stripping, flocculation, sedimentation, soil flushing/washing chelation, etc. Among these, adsorption has evolved as the front line of defense and especially for those, which cannot be removed by other techniques [4]. Additionally, these methods may also affect the generation of secondary wastes, which are difficult to treat. Adsorption is an alternative technology in which increased amount of study has been focused because of cost effectiveness, local availability and technical feasibility for the removal of heavy metal ions from the wastewater [5]. Adsorption of molecules can be represented as a chemical reaction:



Where A is the adsorbate, B is the adsorbent, and $A \cdot B$ is the adsorbed compound. Adsorbates are held on the surface by various types of chemical forces such as hydrogen bonds, dipole-dipole interactions, and van der Waals forces. If the reaction is reversible, as it is for many compounds adsorbed to activated carbon, molecules continue to accumulate on the surface until the rate of the forward reaction (adsorption) equals the rate of the reverse reaction (desorption). When this condition exists, equilibrium has been reached and no further accumulation will occur. Isotherm adsorption models have been used in waste stream treatment to predict the ability of a certain adsorbent to remove a pollutant down to a specific discharge value. When a mass of adsorbent and a waste stream are in contact for a sufficiently long time, equilibrium between the amount of pollutant adsorbed and the amount remaining in solution will develop. For any system under equilibrium conditions, the amount of material adsorbed onto the media can be calculated using the mass balance of Equation below:

$$q_e = V \times \frac{C_0 - C_e}{M_s} \quad (1)$$

where C_0 and C_e (mg/L) are the initial and the final concentrations of adsorbates in flasks, respectively, V is the volume of the solution (in Litres) and m is the mass of dry adsorbent used in grammes [6]. Adsorption isotherms are important criteria in optimizing the use of adsorbents as they describe the nature of interaction between adsorbate and adsorbent. Thus, analysis of experimentally obtained equilibrium data by either theoretical or empirical equations is useful for practical design and operation of adsorption systems. The Langmuir and Freundlich adsorption isotherms were applied to each metal under study.

Moringaoleifera is a multipurpose tree with most of its parts being useful for a number of applications (Figure 1). It is generally used in a number of developing countries as a vegetable, medical plant and a source of vegetable oil. It has an impressive range of medicinal uses with high nutritional value [7]. On the other hand, *Moringaoleifera* seeds have

been found to be a natural coagulant, flocculants, softener, disinfectant, and sludge conditioner[8-10], heavy metal remover in water and wastewater treatment [11-13].

In this study MMOL (biosorbent) is used for CU (II) ions removal from water as a natural alternative for synthetic sorbents. Synthetic water was used to find optimum conditions for water treatment using biosorbent. The effect of biosorbent pH, dosage and time were studied.



Figure 1. *Moringaoleifera* tree.

2. Materials and Methods

2.1. Synthetic Effluents Preparation

An accurate weight of 1.000 g (± 0.0005) CuSO_4 was dissolved in 1 litre of distilled water to produce the stock solutions of synthetic effluent. These stock solutions were then diluted into the required concentrations using distilled water whenever necessary. Every time the stock and standard solution have been prepared, the solution was shaken for about 2 hours using orbital incubator shaker at 30°C and 100rpm to ensure that each solution was homogeneous.

2.2. Sorbents Preparation and Characterization

The *moringaoleifera* leaves (MOL) were removed from the plant and were dried for about 2 weeks. When satisfactorily dried, the leaves were grounded to powder using a mechanical grinder. 80g of the biosorbent was treated with 1600ml, 0.1M HNO_3 with continuous stirring for 2 hours to remove metals from the biosorbent and increase its surface area. Then it was washed with 500ml distilled water, this was done in thrice and the sample was then sun dried for about 6 hours. After the acid treatment, the adsorbent (about 50g) was extracted with 400ml methanol to remove inorganic and organic matter from the sorbent surface. This was carried out for 2 hours 30 minutes. The adsorbent pH was adjusted to 7 using 0.1M NaOH, washed with distilled water, oven – dried for about 1 hour, kept in an air – tight plastic container and put in a refrigerator at 4°C prior the analysis. The MMOL and unmodified *moringaoleifera* leaves (UMOL) samples were characterized thus: specific surface area was determined

using the method of Sear's, [14], the point zero charge (PZC) was determined by solid addition method [15].

2.3. Adsorption Studies

The sorption capacity of the MMOL was evaluated via equilibrium isotherm analysis. The sorption capacities was determined by contacting 50 mL solution of known concentration of CU (II) that ranged between 25 and 300 mg/L with 0.2 g of the adsorbent (MMOL). The mixture was stirred at 200 rpm in thermostatic shaker for 2h, samples were removed, centrifuged, and the supernatant was analyzed for residual CU (II) concentration by using a flame atomic absorption spectrophotometer. The amount of CU (II) sorbed per unit mass of the adsorbent (in mg/g) was calculated using equation 1.

The sorption process variables were optimized thus: the effect of pH on the sorption process was investigated by varying the pH of the initial CU (II) solution between pH 3 – 12; the effect of the adsorbent dose was studied at different dosage of 0.2, 0.4, 0.6, 0.8 and 1.0g of the sorbents in contact with fixed CU (II) solution of 500 mg/L. The mixture in the flask was shaken at 200 rpm for 2h and the equilibrium concentration of the residual CU (II) was determined spectrophotometrically. The CU (II) sorption kinetic parameters, was studied using a range of CU (II) concentrations [25 to 300 mg/l]. A typical experimental procedure was conducted by measuring accurately a liter of the CU (II) solution of known concentration, 2 g of MMOL was added and agitated [at 200 rpm] for 240 min, Samples were withdrawn, at fixed time intervals, centrifuged, and the supernatant was analyzed for residual CU (II) using flame atomic absorption spectrophotometer. The amount of CU (II) sorbed per unit mass of the MMOL [q in mg/g] was calculated using the mass balance procedure.

3. Results and Discursion

3.1. Sorbent Characterization

The modification of MOL produced a material whose PZC value (6.20) was greater than that of the UMOL (3.70). The results of the specific surface area of the UMOL and MMOL showed that the acid treated sample had higher specific surface area (106m²/g) than that of the UMOL (33m²/g). The higher specific surface area of the MMOL could be ascribed to the acid modification of the MOL which opened up the pores.

3.2. Equilibrium Isotherm Studies

The equilibrium concentration between the CU (II) ions in the fluid phase and the CU (II) ions in the MMOL at given temperature was studied and the isotherm parameters obtained by using the linearized models of Langmuir and Freundlich isotherm are presented in Table 1.

$$\text{Langmuir: } \frac{C_e}{q_e} = \frac{1}{Kq_m} + \frac{1}{q_m} C_e \quad (2)$$

$$\text{Freundlich: } \log q_e = \log K_f + \frac{1}{n} \log C_e \quad (3)$$

The values of the monolayer sorption capacities, q_m (mg/g), obtained from Langmuir plot of C_e/q_e vs C_e is 78.45 mg/g while the magnitude of Langmuir constant, K_L , which is the sorption equilibrium constant (dm³/mg) is 1.4642. The higher the magnitude of the heat of sorption, the stronger the bond formed between the sorbate and the sorbent. The Freundlich constant K_f and n which are related to adsorption capacity and sorption intensity respectively, are obtainable from the plots of $\log q_e$ vs $\log C_e$. The values of this constants are presented in Table 1. The value of $1/n$, which is less than unity (0.9463), shows the favorable nature of adsorption of CU (II) on MMOL. The description of the sorption of CU (II) on MMOL by the Freundlich isotherm equations is an indication of the heterogeneity of the surface with a non-uniform distribution of heat of adsorption over the surface of the MMOL. The linear coefficient of determinations, r^2 , was used to evaluate the fitness of each isotherm equation to the experimental data obtained from the optimization process employed.

Table 1. Equilibrium Isotherm Parameters of sorption of CU (II) on MMOL.

Langmuir isotherm parameter			Freundlich isotherm parameter		
q_m (mg/g)	K_L	r^2	K_f (1/g)	$1/n$	r^2
78.45	1.4642	0.996	53.44	0.9463	0.998

The values of r^2 obtained when the experimental data were fitted into Langmuir isotherm equation was lower than that of Freundlich isotherm equation. The description of the sorption of CU (II) on MMOL by the Freundlich isotherm equations is an indication of the heterogeneity of the surface with a non-uniform distribution of heat of adsorption over the surface of the MMOL. The results of the comparison of the Langmuir sorption capacity (q_m) obtained from the present study with the values obtained by other researchers from the use of other sorbents for the removal of CU (II) ions from aqueous solution is presented in Table 2. The result indicated that MMOL compared favorably with the other adsorbents that have been used and the Langmuir sorption capacity was higher than some of the other adsorbents.

Table 2. Comparison of the Lagmuir sorption capacity (q_m in mg/g) of different sorbents for CU (II).

ADSORBENTS	q_m (mg/g)	References
Modified silica aerogel	90.1	[16]
Amino functionalized Fe ₃ O ₄ @SiO ₂ core-shell NPs	29.85	[17]
Cross linked chitosan with		
Epichlorohydrin	35.46	[18]
a loofa sponge (FBILS)	98.9	[19]
Modified moringa oleifera leaves	78.45	[This work]

3.3. Sorption Kinetics Studies

The initial CU (II) ions concentration was studied to observe if the initial concentration of CU (II) ions would have an influence on the sorption process. In the range of CU (II) ions concentration studied, the uptake of the CU (II) was

rapid in the first 50 min. The rapid uptake then gave way to a much slower adsorption after 50 mins (Figure 2). This initial rapid uptake can be attributed to the concentration gradient created at the start of the adsorption process between solute

concentration in solution and that of the MMOL surface. As the CU (II) loading increases this gradient reduces and gives way to slower uptake and there is no change in adsorption on further increase in contact time.

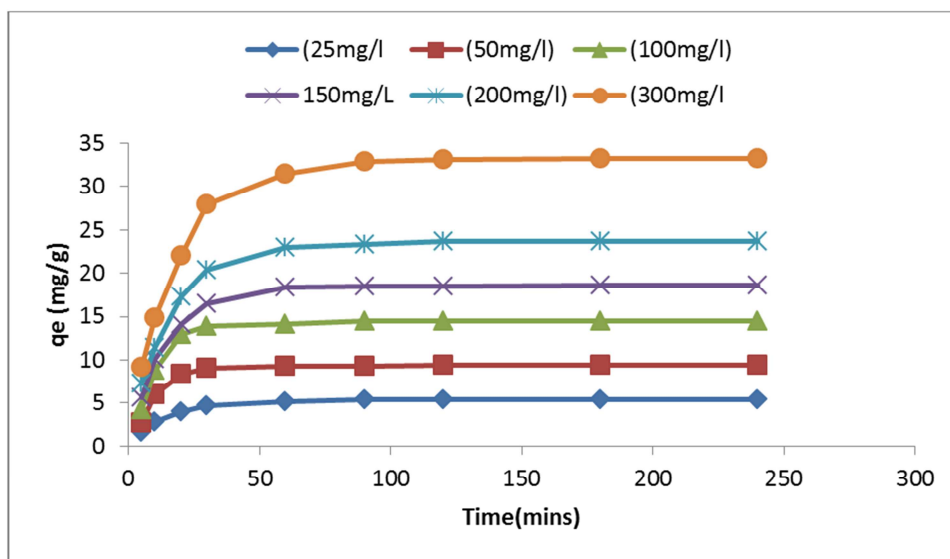


Figure 2. Effect of initial CU (II) concentration (mg/l) and time on the sorption of CU(II) by MMOL.

In order to study the mechanism of sorption and potential rate determining steps, pseudo first and second order kinetic models was used to test the experimental data obtained from the variability of the initial CU (II) ions concentration. pseudo first-order equation 4, and pseudo second-order equation 5, were tested with the data obtained from the kinetic studies, thus:

$$\log[q_e - q_t] = \log[q_e] - [k/2.303]t \quad (4)$$

$$t/q_t = 1/kq_e + 1/q_e t \quad (5)$$

The plots obtained for these kinetic models are presented in Figure 3 and Figure 4 respectively.

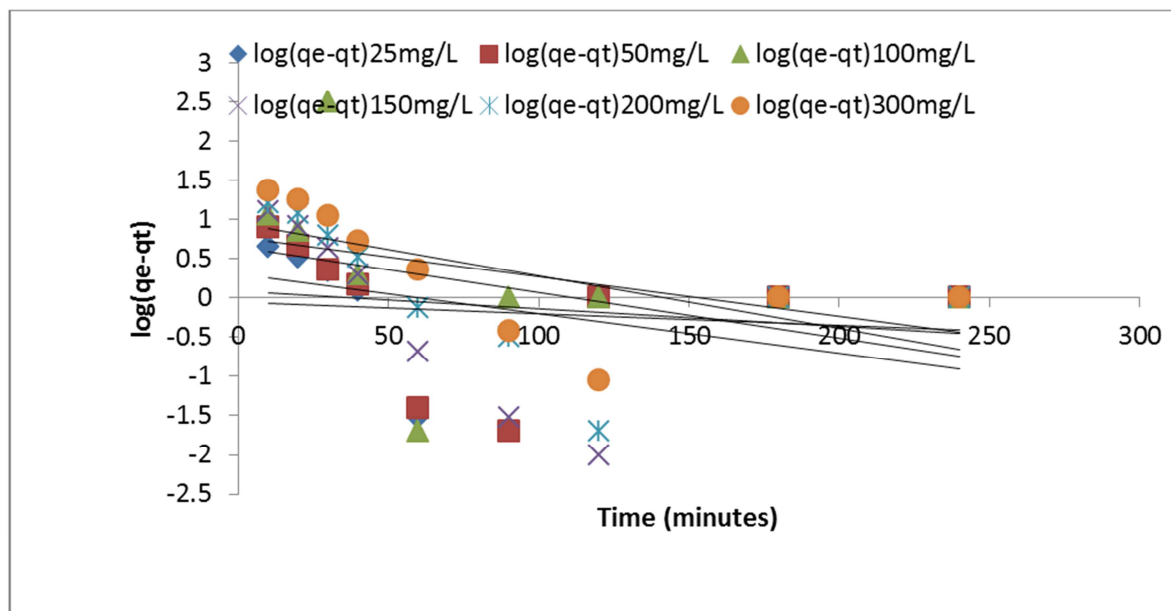


Figure 3. Pseudo-first-order kinetic plots for the removal of CU(II) by MMOL at different initial CU(II) concentration.

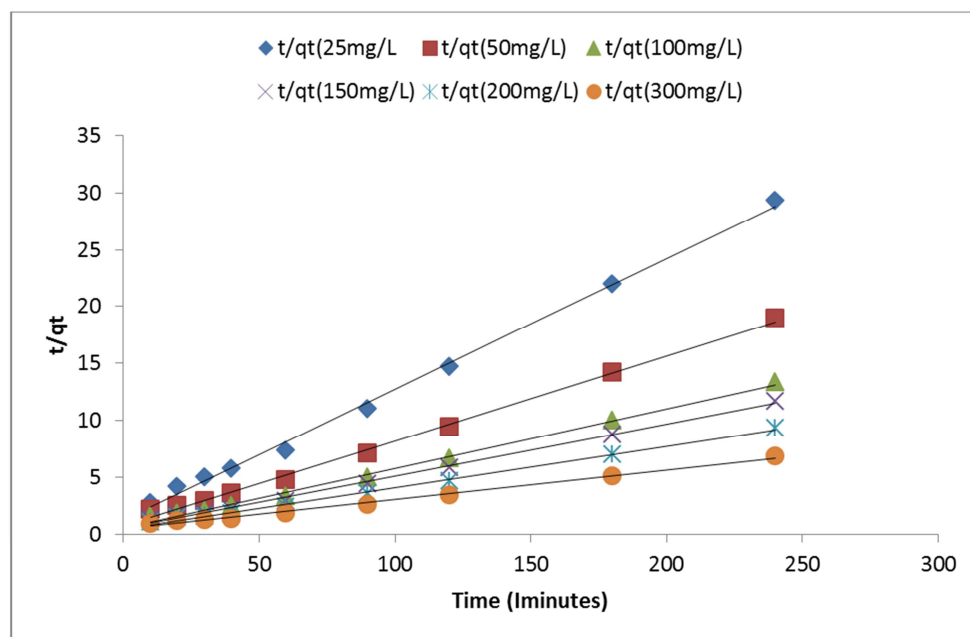


Figure 4. Pseudo- second-order kinetic plots for the removal of CU(II) ions by MMOL at different initial CU (II) concentration.

The results from the analysis of the data obtained from these plots are presented in Tables 3. The experimental data showed better fitting to pseudo second order ($r^2=0.993 - 0.997$).

Table 3. Kinetic Parameters of CU (II) Sorption on MMOL.

Initial Conc.	Pseudo first order			Pseudo second order		
Mg/L	q_{e1}	K_1	r^2	q_{e2}	K_2	r^2
25	2.3×10^{-3}	3.6×10^{-3}	0.018	8.6956	0.0932	0.997
50	4.6×10^{-3}	4.3×10^{-3}	0.039	13.5135	0.0864	0.996
100	11.5×10^{-3}	5.9×10^{-3}	0.127	19.2308	0.0611	0.995
150	11.5×10^{-3}	10.5×10^{-3}	0.136	22.2222	0.0583	0.996
200	11.5×10^{-3}	12.8×10^{-3}	0.261	27.7778	0.0579	0.995
300	13.8×10^{-3}	15.4×10^{-3}	0.419	40.000	0.0567	0.993

This is a pointer to the fact that the sorption of the CU(II) ions moieties on MMOL occurred via chemisorptions. If the sorbate uptake is chemically rate controlled, then the pseudo second order constants will be independent of particle diameter and flow rate will depend on concentration of the ions in solution [20]. A review of the results, presented in Tables 3, showed that the pseudo second order parameters obtained from the uptake of CU(II) ions onto MMOL (q_e and k_2 values) varied with the initial CU (II) concentration.

3.4. Effect of Adsorbent Dosage

The effect of the adsorbent dose on the sorption of copper (II) from aqueous solution onto MMOL was carried out. The result showed that the sorptions of CU (II) are functions of MMOL dosage. Increasing the dosage of the MMOL and keeping the CU(II) concentration constant makes a large number of sites available for a fixed concentration of sorbate. This is anticipated because an increase in MMOL dosage will lead to an increase in the quantity of sorption sites available for sorbent-sorbate interaction [21]. Meanwhile a reverse trend was observed in the loading capacity (q_t) when the linear form of Langmuir equation was used to analyzed the

isotherm experiments and the results obtained are presented in Table 4.

Table 4. Effect MMOL dosage on the sorption of CU(II).

Sorbent dose	q_m	K_L (mg/g)	r^2
0.2	78.45	1.4642	0.998
0.4	65.39	1.6745	0.993
0.6	61.72	1.7231	0.985
0.8	53.82	1.9367	0.987
1.0	38.66	1.9876	0.988

The results showed that as the MMOL dose was increased from 0.2 to 1.0 g/L, a reduction was observed in the values of the monolayer sorption capacities, q_m , from 78.73 to 38.66 mg/g. The reduction in the sorbent capacity with increase in dose could be attributed to two reasons: the increase in sorbent dose at constant CU [II] ions concentration and volume will lead to unsaturation of sorption sites through the sorption process [22-24] and secondly may be due to particulates interactions. Such aggregation would lead to a decrease in total surface area of the sorbent and an increase in diffusional path length [22]. The value of the sorption equilibrium constant, K_L , increased with increase in the sorbent dose.

3.5. Effect of pH

The pH of the medium of interaction between the sorbent and the sorbate is an important parameter in any adsorption process. This dependence is closely related to the acid-base properties of various functional groups on the adsorbent surfaces [25]. The change of pH affects the adsorptive processes via the dissociation of functional groups on the active sites of the adsorbent. This subsequently leads to a shift in the reaction kinetics and equilibrium characteristics of the adsorption process [26]. An increase in metal adsorption with increasing pH values can be explained on the basis of competition between the proton and metal ions for the same functional groups, and a decrease in the positive surface charge, which results in a higher electrostatic

attraction between the biosorbent surface and the metal [27]. Low pH conditions allow hydrogen and hydronium ions to compete with metal binding sites on the biomass, leading to poor uptake. Biomasses are materials with an amphoteric character; thus, depending on the pH of the solution, their surfaces can be positively or negatively charged. At pH values greater than the point of zero charge ($pH > PZC$), the biomass surface becomes negatively charged, favoring the adsorption of cationic species. However, adsorption of anionic species will be favored at $pH < pH_{pzc}$. The pH_{pzc} of the MMOL is between 6.0 and 6.2, indicating that the surface of the biosorbent presents acid characteristics. The surface charge of the MMOL is positive at $pH < PZC$, is neutral at $pH = PZC$ and is negative at $pH > PZC$.

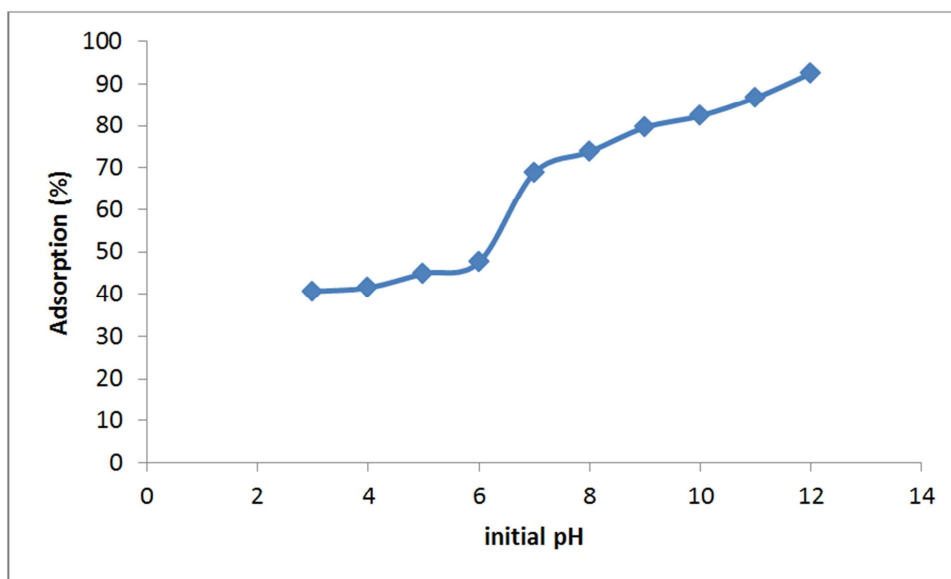


Figure 5. Effect of pH on the sorption of CU (II) ions onto MMOL.

4. Conclusion

The capacity of MMOL to remove CU(II) ions from aqueous solution was investigated using equilibrium isotherm analysis. Langmuir and Freundlich isotherm equations were used to describe the sorption process. Freundlich isotherm equations had the best correlations amongst the two isotherm equations used. This shows the heterogeneity of the surface of the MMOL and the multilayer adsorption nature of the CU(II) ions on MMOL. The effect of initial CU(II) ions concentration and MMOL dosage on the sorption dynamics of CU (II) on MMOL was studied. The experimental data obtained from the studies were fitted to pseudo first and pseudo second order kinetic models and the results showed an extremely high coefficient of determination (r^2) when it was fitted to the pseudo second order kinetic models. Also increase in the MMOL dose at fixed CU (II) concentration caused a reduction in the amount of CU (II) ions sorbed due to an increase in the large number of sites that are ready for CU (II) adsorption. Moreso, CU(II) ions solution pH must be optimally selected to obtain the highest possible removal of

CU (II) ion. As shown by the results, CU (II) sorption onto MMOL increases with increase in pH of the CU (II) solution.

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