
A Review on Different Cooling/Lubrication Techniques in Metal Cutting

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Abstract: Various types cooling/lubrication techniques are used in machining processes for enhancing machining performances. Conventional way of cooling/lubrication requires higher coolant cost, waste and disposal cost. Not only has that it had many negative impacts on environment and operators health. For attaining highest efficiency of cutting fluids with minimum quantity, different sustainable strategies are tried to develop. In recent decades researchers are worked out on different cooling/lubrication strategies alternative to conventional cooling. This paper represents a comprehensive review of all presently practiced cooling/lubrication strategies and their effects on different aspects such as surface quality of machined component, tool wear, tool life, cutting temperature, cutting forces etc. through analyzing selected papers. The influence of different cutting fluids such as solid lubricants, nanofluids, ionic liquids etc. with their positive and negative impacts is also discussed. The research gaps are also identified for further research works. From review it is clear that the machining performance is highly affected by cooling techniques and coolant types. Selection of proper cooling technique with suitable cutting fluids depends on work material, tool material and cutting variables.

Keywords: Flood Cooling Conventional Cooling, Mist Cooling, High Pressure Cooling (HPC), Minimum Quantity Lubrication (MQL), Nanofluids, Ionic Liquids, Cryogenic Cooling, Hybrid Cooling

1. Introduction

Dry machining or machining with no cutting fluids is the most common and clean manufacturing approach but higher cutting variables restrict the applicability of this process. Work hardening, plastic deformation of chips, higher tool wear, poor surface quality are some of the major negative impacts of dry cutting. In dry machining an enormous amount of power is lost due to heat generation between tool surface and workpiece by plastic deformation and by friction between tool/chip on the rake and flank faces. It has been observed that about 20-30% power is lost due to generation of heat [1]. So, it is clear that necessity of metal working fluids is unavoidable in machining. The major functions of metal working fluids are shown in Figure 1. But in conventional cooling/lubrication the requirement of cutting fluids is approximately 10-100 L/min [2] that is needed to minimize for attaining sustainability. In recent years for eliminating or reducing this harmful effects

and attaining sustainability, researchers have been trying to improve cooling/lubrication technology alternative to conventional cooling techniques.

Near dry machining (NDM) or minimum quantity lubrication (MQL), cryogenic cooling are some efficient cooling/lubrication techniques alternative to conventional cooling. Applicability of these alternative techniques is described in following sections in brief. Very earlier stages of cutting process, cutting fluids are considered as a substance such as oil or water that can cool/lubricate. Taylor applied water as a cutting fluid in 1907 for machining hard to cut metals with 40% increased cutting speed [3]. But now many types of cutting fluids such as oil based fluids (straight cutting oil), water based fluids (synthetic, semi-synthetic or emulsion type), gaseous based fluids, solid lubricants, nanoparticles, gels, paste, and aerosols etc. are used for cooling/lubrication. Selection of cutting fluids depends on the complexity of process, workpiece and tool material, cutting variables etc. Cutting fluids having higher heat dissipation ability, proper

wetting capability, proper formation of lubricating film is considered as a better coolant/lubricant. Gaseous coolants are kept in gas form at room temperature but they are used in machining as high pressurized fluids.

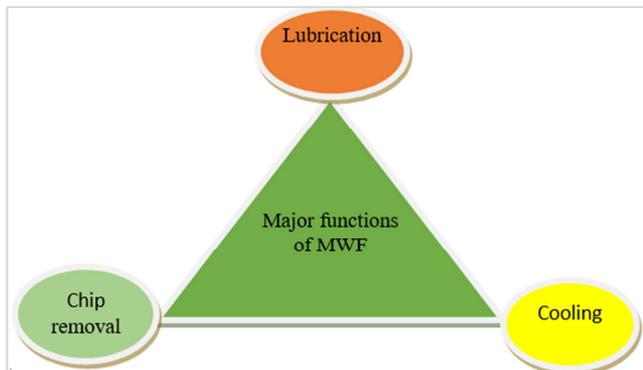


Figure 1. Major functions of metal working fluid (MWF).

Normally argon, helium, carbon-di-oxide, nitrogen are used as gaseous [4]. Higher cost of gas based lubricants restricts its use.

In recent decades researchers have given their focus on increasing the use of biodegradable, nontoxic, environment friendly lubricants/coolants. Recently mineral oils or petroleum based oils are tried to replace for their higher toxicity, non-biodegradability and harmful impacts on environment. Synthetic oils, vegetable oils, solid lubricants, nano lubricants are highly used by researchers. Ionic liquids are tried to use as lubricant additives in cutting processes. Many researchers have already discussed different cooling/lubrication techniques in various machining processes. Chinchanikar and Choudhury [5] provided a literature review on machining hardened steel using coated tools under dry or other cooling/lubrication techniques. Chetan *et al.* [6] represented a detail review on sustainable techniques to make cutting processes environment friendly and cost effective. Debnath *et al.* [7] pointed out vegetable oil as bio-based oil and reviewed its development. Minimum quantity lubrication (MQL) and cryogenic cooling are also reviewed. In another review Sharma *et al.* [8] concluded that systematically application of minimum quantity lubrication (MQL) with nanoparticles can improve productivity and enhances the cutting quality. Benedicto *et al.* [9] presented a detail technical, economic and environmental impact analysis of cutting fluids in cooling/lubrication in machining. They recommended employing vegetable oils as sustainable cutting fluids with proper treatment. Krolczyk *et al.* [10] performed a comprehensive analysis on balanced use of cutting fluids for difficult to cut metals such as Titanium, nickel and chromium based alloys machining. They represented a review on ecological trend in machining processes. But this paper presents a comprehensive literature review on recent advancement of alternative cooling/lubrication strategies to conventional cooling with newly developed cutting fluids such as nanofluids, ionic liquids and their effects on machining performances. Moreover hybrid

cooling/lubrication techniques are also described in brief which are not available in other previous review works. The reviewed cooling/lubrication approaches are illustrated in Figure 2 and all the short form of used terms are listed in Table 6 with their correct abbreviations.

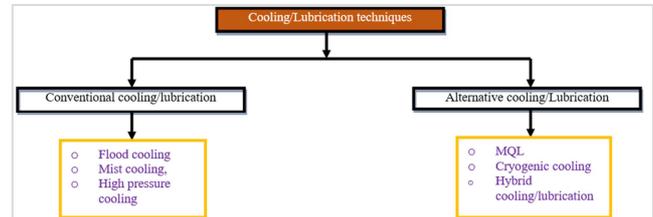


Figure 2. Classifications of discussed cooling/lubrication techniques.

2. Conventional Cooling/Lubrication Techniques

Cutting fluid is used as an additive in machining processes for increasing productivity. Various cooling/lubrication approaches are followed for applying cutting fluids into cutting zone. Conventional cooling/lubrication can be grouped into three classes-wet/flood cooling, mist cooling and high pressure cooling (HPC) [7] which are described below.

2.1. Flood Cooling

Flood cooling is also named as wet cooling. This process requires cutting fluids approximately 20 L/min [11] and in general the tool is flooded with steady flow of cutting fluids in the clearance face under 300kPa pressure or more for achieving better results [12]. But it is found that operators who are in physical contact in cutting fluid suffer almost 80% diseases [13]. Flood cooling is now tried to avoid in machining due to higher cost of coolants/lubricants for massive use, negative effects on operators health and environment, complexity of huge waste disposal.

2.2. Mist Cooling

In mist cooling water based coolants are mainly applied through a nozzle with high pressurized air to the cutting zone for reducing cutting temperature and increasing tool life. Babic *et al.* [14] tried to remove the cost and disposal of expensive coolants by mixing air and water as coolant in grinding process. They proved that mist jet cooling is an effective alternative to flood cooling and easier to clean. An *et al.* [15] studied the effect of cold water mist jet (water at 0°C and high pressurized (0.6MPa) air (-20)) cooling on turning Titanium TC9 alloy. They compared this cooling technique with flood cooling and cold air jet based on cutting temperature, tool wear and surface roughness. The higher forced convection, high pressurized jet impingement and vaporization effect accelerates the heat transfer in cold water mist jet cooling. Lv *et al.* [16] applied pneumatic mist jet cooling in milling burn resistant Ti40 alloy. The required quantity of mist coolant is 96ml/min which is smaller than total flood cooling (2.52 L/min). At variable cutting speeds

(30, 60, 80, 100 m/min) total flood cooling and pneumatic mist jet cooling was compared based on flank wear, cutting temperature, tool life and material removal volume. All types of wear such as adhesion, micro-chipping, notch wear, coating delamination were reduced except cracks in this new cooling technique. Nandgaonkar et al. [17] performed dry drilling and ester oil based water oil mist spray (WOMS) drilling of Ti6Al4V alloy at 50m/min cutting speed with 167mm³ material removal rate using TiAlN coated twist drill. Approximately 66% higher tool life was achieved in water oil mist spray cooling than dry drilling.

Mist cooling requires less coolant flow so its environment friendliness and efficiency is higher than flood cooling. Now researchers are trying to introduce new type mist coolant such as nitrogen oil mist cooling, cold compressed nitrogen mist cooling etc.

2.3. High Pressure Cooling (HPC)

In flood cooling improper penetration of cutting fluid to cutting zone generates higher temperature in machining difficult-to-cut metals at a higher cutting speed. Kaminski and Alvelid [18] pointed out that this higher temperature generates vapor barrier through vaporizing the applied coolant so the cooling effect is reduced. High Pressure Cooling (HPC) is a technique to penetrate the coolant at the cutting zone at higher pressure (5.5–35MPa) through nozzle [7]. Ezugwu and Machado [19] used HPC supply of coolant at 14MPa pressure for machining Inconel 901 alloy for eliminating the built up edge chips formations and after successful implementation better tool lives with no built up edges was found. The equipment's required for HPC installation are high pressure pump, high pressure tubing and an outlet nozzle attached to side of tool holder. The high pressurized jet can be applied in two ways: external cooling and internal cooling [20]. Colak [21] applied high pressure cooling in Ni based alloy machining and found that pressure of coolant has a strong relationship with flank wear. The author also pointed out that high pressurized coolant flow reduces temperature and cutting force through proper penetration at deeper cutting zone so tool wear is reduced. Colak [22] again studied the performance of HPC in turning of Titanium alloy in respect of tool life, material removal rate and surface roughness. Only tool life was almost 112% higher in HPC at 300bar coolant pressure than flood cooling. Kramar and Kopac [20] conducted an experiment for showing the effect of jet pressure and flow rate in machining C45E steel and Inconel 718. For both metals machining, conventional cutting speeds and coated tools were used. Under these conditions HPC increased tool life and chips breakability. Xu et al. [23] experimentally showed the cooling mechanism of high pressure cooling (HPC) using finite element modeling (FEM) and the effect of pressure on tool wear, cutting force and chip structure. It is pointed out that with increasing pressure rate air bubbles disappear from tool surface and 22% temperature was reduced with 89% increased tool life at 10MPa jet pressure. Alaxender et al. [24] concluded that HPC minimizes 50% consumption of cutting fluid and also reduces cutting temperature and cutting force. Cayli et al.

[25] designed a special jet guidance geometry tool for increasing energy efficiency of HPC in machining hard to cut metals Inconel 718 and Ti6Al4V. The experimental results revealed that the modified jet guidance geometry reduced 41% tool temperature than conventional tool. The authors pointed out that efficiency of energy consumption can be achieved through proper adjustment of flow rate and pressure of coolant with minimum consumption of hydraulic power and electric power. Alagan et al. [26] checked out the performance of HPC using different textured carbide tools. The results showed that combination effect of texturing at both rake face with dimples and flank face with pyramids provides 30% better tool life in machining alloy 718 under experimental conditions. Busch et al. [27] performed a comparative analysis among HPC, cryogenic cooling and aerosol dry cooling (ADL). The researchers noticed that at higher cutting speed highest tool life was achieved using HPC but in contrary energy consumption was highest in HPC so this cooling was suggested for roughing operations. Sørby and Vagnorius [28] claimed that HPC cooling technique is unable to increase tool life, minimize notch wear and edge chipping as well as to reduce cutting force in machining Inconel 625 using ceramic insert under 5-15MPa coolant pressure at 200-300m/min cutting speed. They concluded that HPC technique is not suitable for machining using ceramic tools. Ezugwu and Bonney [29] performed HPC at a pressure of 11-20MPa on Inconel 718 machining with SiC-whiskers reinforced ceramic tools. The result concluded that HPC is responsible for severe edge notching, shorter tool life, increasing cutting force with improving chip breakability. In another paper, Ezugwu et al. [30] performed HPC repeatedly under finishing conditions and showed that tool life is increased within 11-15 MPa pressure and dropped at a pressure 20MPa with cutting speed 300m/min.

From discussed review it is clear that due to higher pressure HPC facilitates breakability of chips, reduces tool wear and cutting temperature, increases tool life and productivity. HPC is mainly suggested for machining hard to cut metals due to its higher cost. Tool geometry and texturing are also influential in HPC.

3. Alternative Cooling/Lubrication Techniques

The development and effect of different cooling/lubrication techniques alternative to conventional cooling are discussed in this section.

3.1. Dry Machining

The growing demand of sustainable machining drives researchers to find out promising cooling/lubrication techniques. In today's manufacturing world dry machining is gaining more importance for avoiding health hazards caused by coolants or lubricants. But in most practical situations tool wear is drastically increased with increasing cutting speed because of higher heat which is generated from 99% energy consumption of tool during

plastic deformation [31]. Raykar *et al.* [32] investigated the comparative effects of dry cutting and cutting with suitable coolant on surface topography of EN8 and found no significant difference for surface roughness between these two techniques. They pointed out that dry cutting may be performed under favorable cutting condition. Rubio *et al.* [33] performed dry machining and MQL with different flow rates on magnesium UNS M11917 pieces for comparative analysis based on surface roughness. At low feed rates MQL provided better surface finish with 4.5ml/h flow rate but with increasing feed rate dry machining produced better surface quality than MQL. Dry machining of Aluminum alloy is another critical task because of its low melting point and higher ductility. Aluminum adheres to tool material and built up edge is formed in absence of cutting fluid. During dry cutting of Aluminum alloy wear such as adhesion, built up layer (BUL), built up edge are formed more drastically at higher cutting condition [34]. So special attention must be provided for selection of tool materials, tool geometry, coating materials in case of machining difficult to cut materials where extreme heat, tool wear is generated. C. Bermudo *et al.* [35] performed parametric analysis of dry turned UNS A-97075 alloy using uncoated WC-CO insert. No regular relation between feed and ultimate tensile strength was observed. In recent years coating technology is becoming more attractive alternative to conventional cooling/lubrication not only for assuring sustainable machining but also for increasing tool life and surface integrity of work materials especially for difficult to cut metals. Davoodi B. *et al.* [36] claimed that using coated carbide insert for aluminum alloy can be turned without use of cutting fluids through experimentation. Devillez *et al.* [37] demonstrated that dry machining of Inconel 718 by coated tool at 60m/min cutting speed, 0.1mm/rev feed and 0.5mm depth of cut can provide better surface quality with acceptable microhardness and no significant microstructure alteration was found. Venkatesan and Thakur [38] investigated the surface integrity of Nimonic 263 alloy in dry machining using Physical Vapor Deposition (PVD) and Chemical Vapor Deposition (CVD) coated carbide inserts. From experimental results it is proved that PVD coated carbide inserts perform better than CVD coated inserts at medium range values of cutting parameters. Besides this coating technology many researchers adopted surface engineering approach for enhancing the property of tool materials by textures. Sugihara *et al.* [39] developed dimple texture on noncoated WC-CO insert in face milling and represented the comparative analysis between conventional cutting tool and newly designed tool. Experiments were also performed for different textures with their various directions, percentage of area texture, sizes of micro dimples. The results indicated that micro dimples texture provides more versatility. Niketh and Samuel [40] performed drilling under margin textured, flute textured and non-textured carbide drill tools and 10-12% reduced thrust force was found in dry drilling using margin textured tools.

From above described review results it can be summarized that sustainability of dry machining is highest because no cutting fluid is used. But some limitations such as high rate of wear, higher friction, and poor surface quality, built up edge formation motivate researchers to modify dry machining. Use

of different textured tools, application of PVD or CVD coated tools and surface engineering are some of the improvements of dry machining.

3.2. Minimum Quantity Lubrication (MQL)

Dry machining is most sustainable but it has some limitations which are already discussed. Minimum Quantity Lubrication (MQL) or Near dry machining (NDM) is one of the most promising solutions to meet this requirements because in Minimum Quantity Lubrication (MQL) or near dry machining (NDM), a minute quantity of fluid (10-100 ml/h) is sprayed to cutting zone with compressed air [41] which is middle between flood cooling and dry machining. Some researchers [42-43] worked out on optimizing MQL parameters such as droplet size, wetting angle, wettability, nozzle distance, nozzle angle, flow rate etc. are also influential factors for enhancing the spray quality. Many researchers have been analyzing the effect of MQL on tool life, tool wear, surface integrity of work materials, cutting force, specific energy in various machining processes for different materials. Sarikaya and Güllü [44] focused on Taguchi method, RSM and desirability function for identifying the effect of cutting parameters and cooling conditions on surface roughness of AISI 1050 steel. The results narrated that cooling condition has greater impact on surface roughness. Rahim *et al.* [45] investigated the efficiency of MQL over dry machining in turning of AISI 1045 at higher cutting speed 250~350m/min. The results revealed that in MQL the cutting temperature was reduced 10%-30% and as well as tool chip contact length was reduced 12% due to proper cooling effect of air consistent aerosol flow, cutting force was reduced by 5% to 28% due to lubrication effect of synthetic ester and also thinner chips were produced than dry turning. Better surface quality was achieved in MQL at 200m/min cutting speed. Dureja *et al.* [46] suggested MQL as an alternative to dry and flood cooling for sticky material stainless steel in case of minimizing tool wear and surface roughness based on experimental and numerical results. Sankar and Choudhury [47] employed dry air cooling, flood cooling and lubrication using minimum quantity cutting fluid in turning highly alloyed steel. Emulsion type mineral oil was used as lubricants. The experimental results revealed that lubrication using minimum quantity cutting fluid may be an economic and eco-friendly alternative to flood cooling. Similarly Nouioua *et al.* [48] compared the performance of dry, wet and MQL cooling for machining X210Cr12 using CVD coated carbide insert and 23~40% improvement of tool life was found under MQL. After experimentation they also concluded MQL as a greener, cost effective and safe approach of lubrication. Ekinovic *et al.* [49] presented an statistical report of costing related to manufacturing and found approximately 15% cost is related with application and disposal of cutting fluids represented in Figure 3. Using oil on water droplet (mixing ratio 10 ml/h of oil and 1.7 L/h of water) MQL 17% reduced cutting force in turning of low carbon steel St52-3 was achieved. In drilling chip extraction is a major problem which adversely affects the surface integrity of drilled holes. Brinksmeier *et al.* [50] applied MQL with

variable pressures in low frequency vibration assisted drilling and observed chip breaking technique under dry condition, compressed air with variable pressure and compared with MQL. They found that MQL with 6 bar pressure provided highest chip extraction index at lower feed and higher amplitude of low frequency vibration assisted drilling. Tamang et al. [51] analyzed sustainability of dry machining and MQL for machining Inconel 825 alloy. MQL reduced surface roughness, tool wear and power consumption by 10.41%, 16.57% and 8.47%, sequentially than dry machining.

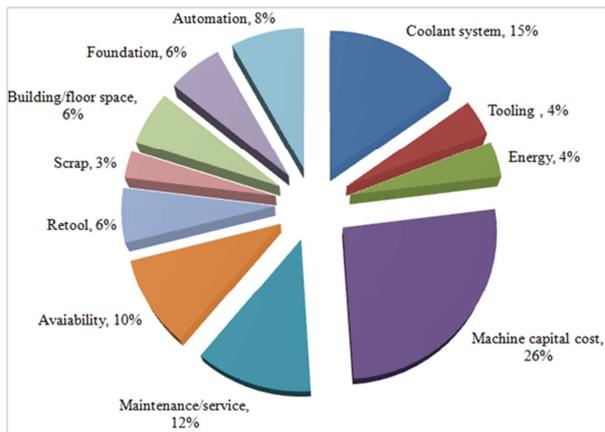


Figure 3. Distribution of manufacturing cost in conventional cooling (Redrawn: Ekinovic et al., 2015).

Khatri and Jahan, [52] investigated different types tool wear in milling Ti6Al4V alloy under dry, MQL and flood cooling techniques and found comparatively less tool wear in MQL. MQL enhances the environmental sustainability as well as other economic aspects. Magnesium alloy is used in aeronautical sectors for its lightness property but its machining is very critical. Water based lubricants may generate flammable atmosphere and higher speed may burn the generated tiny chips. Viswanathan et al. [53] performed turning of magnesium alloy using uncoated carbide insert under dry and MQL and analyzed the results using Taguchi technique and Grey Relational Analysis method. From both statistical analyses better outputs were obtained for MQL. Chetan et al. [54] developed a mathematical model of

measuring specific cutting energy under MQL. Validation of model was checked out in case of turning Ni based Nimonic 90 alloy under MQL and it was found that 250ml/h flow rate of MQL reduced specific cutting energy 50% per unit volume of secondary shearing zone due to high pressurized droplet flow into shear zone.) Besides the benefits, MQL has limitations in deep hole drilling, energy intensive processes such as grinding, machining hard to cut metals, proper cooling and chip evacuation process applications [55]. Some researchers found some limitations of MQL in cooling purposes which are also reviewed. Sakharkar and Pawade [56] concluded that MQL provides better lubrication, reduces surface roughness, tool wear but it is not a suitable cooling technique at higher speed. Hadad and Sharbati [57] formed finite element model (FEM) and also experimentally showed that MQL is not able to reduce temperature of grinding process significantly. Chakule et al. [58] performed grinding of high carbon chromium D3 steel under flood cooling and MQL and used soluble oil in both cooling techniques. The authors found that cutting force, cutting temperature and specific energy was lowest for wet cooling than dry and MQL. But better surface quality was achieved in MQL.

From above review results it is clear that MQL is economic and safe lubrication technique but its cooling effect needs to be improved. For enhancing cooling property of MQL in recent years some modifications are executed such as MQL with ionic liquids, MQL with modified vegetable oil, MQL with solid lubricants, MQL with nanofluids and MQL with ionic liquids etc which are described in next sub-sections.

3.2.1. MQL with Vegetable Oil

Vegetable based cutting fluid has opened a path to enhance MQL sustainability because it is nontoxic, renewable and easily biodegradable. The anti-wear and friction properties can be increased by proper use of additives. The synthesized vegetable oil has better cooling and lubrication properties. Triglycerides of vegetable oil provide strong lubrication film. Vegetable oil is also a good coolant because of its high heat conductivity (0.17W/m.K) which is greater than mineral oil (0.125 W/m.K) [59]. All the discussed research works with findings in this section are listed in Table 1.

Table 1. Summary of published research works on Minimum Quantity Lubrication (MQL) using vegetable based oils

Findings	MQL using coconut oil (wetting angle 33.7°) significant decrease in friction coefficient, tool wear, along with favorable chip morphology and better surface quality of the workpiece.	Tool life for flood cooling, MQL is 314s but for air blow is only 40s Tool wear rate is almost same for MQL and flood cooling so MQL be an alternative to flood cooling.	Ultimate Tensile strength is increased 28% at MQL condition with 260m/min. The grain size is finer at MQL than dry.	Wear is reduced in MQL with 150m/min speed.
Machining Environment	MQL, dry and flood cooling	MQL, flood cooling and air blow	Dry and MQL	Dry and MQL
Machining Process	Turning	Drilling	Milling	Turning
Coolant types	Coconut oil; Soluble oil	Soluble oil, Synthetic ester, palm oil	Rapeseed oil	LB 2000
Used materials	AISI 1040	Ti6Al4V	Friction stir welded Al 6061	SAE 1045 steel
Authors	Vardhaman et al. (2018)	Rahim and Sasahara (2011)	Al-Wajidi et al. (2018)	Sampaio et al. (2018)

Table 1. Continued.

Findings	Surface quality was enhanced by MQL with aloe Vera oil than MQL with mineral oil.	Better tool life with less cutting force was found in MQL with vegetable oil.	MQCL reduced cutting temperature and friction between tool/chip and tool/work piece.	Modified jatropha oil may be an alternative to synthetic ester.	Modified jatropha oil with 0.05% hexagonal boron nitride (hBN) reduced surface roughness, tool wear, cutting temperature and cutting force.
Machining Environment	MQL	MQL	Dry and MQCL	MQL	MQL
Machining Process	Turning	Milling	Down milling	Turning	Turning
Coolant types	Aloe vera oil	Vegetable oil	Bescut 173	Jatropha oil, synthetic ester	Jatropha oil and synthetic ester
Used materials	M2 steel	Waspaloy	Inconel 718	AISI 1045	AISI 1045
Authors	Agarwal and Patil (2018)	Yildirim et al.(2017)	Zhang and Wang (2012)	Talib and Rahim (2015))	Talib and Rahim (2018)

(Rahim and Sasahara [60] analyzed the efficiency of MQL using palm oil over MQL with synthetic ester and flood cooling in High speed drilling of titanium alloy. The study enlightened the efficiency of MQL over air blow and flood cooling. The study also pointed out that heat generation; torque and cutting force are lower for MQL using palm oil than MQL using synthetic ester because of higher viscosity of palm oil (40mm²/s). Yildirim et al. [61] compared the efficiency of vegetable oil over synthetic, mineral and mineral-synthetic oils with different flow rates in milling using Taguchi approach.

Analytical results showed that vegetable oil provides better tool life and less cutting force than other selected oils. In MQL tool life was 314s which was only 40s for air blow cooling. Actually this result proves that proper penetration of small quantity of oil can reduce the temperature highly than air blow where lubrication and cooling effect is very poor. Cooled air is supplied as add-ons in MQL for improving its cooling properties. Zhang and Wang [62] performed end milling of Inconel 718 under dry condition and MQL with compresses cooled air or MQCL using vegetable oil as a base oil. The experimental results showed that tool life is approximately 1.57 times larger of MQCL than dry milling and lower cutting force is achieved due to superior cooling and lubrication. Al-Wajidi et al. [63] evaluated that MQL with rapeseed oil improve the microstructure of friction stir welded (FSW) Al 6061 alloy and increases the ultimate tensile strength almost 28% than dry machining. Sampaio et al. [64] have been doing their experiments on MQL with LB2000 vegetable based cutting fluid for induction hardened SAE 1045 steel machining and found reduced wear. Agrawal and Patil [65] experimentally investigated the performance of non edible aloe-vera oil and compared with mineral oil in turning molybdenum high speed steel M2. Experimental results reveal that MQL using aloe vera oil provides 0.14% reduction of tool wear and 6.7% reduction of surface roughness. Vardhaman et al. [66] applied coconut oil as a cutting fluid in MQL and performed a comparative analysis among dry, wet, and coconut oil, MQL with soluble oil and MQL with coconut oil. The researchers also concluded that the lubrication property is higher for coconut oil because wettability area of coconut oil droplet is more than the rest of oils in experiment. Various

types of vegetable oil are available in commercial market so selection of suitable one is critical. For plain grinding of nickel base alloy GH4169 seven types of vegetable oil such as castor oil, palm oil, corn oil, soybean oil, sunflower oil, rapeseed oil and peanut oil are analyzed. Noticeable point is that viscosity has significant influence on heat transfer and energy ratio coefficient. Talib and Rahim [67] chemically modified crude jatropha oil to trimethylpropane ester (modified jatropha oil) and proved that this modified oil be a substitute of synthetic ester in MQL. In another research, Talib and Rahim [68] added hexagonal boron nitride (hBN) in different percentages and achieved better machining performance from modified jatropha oil with 0.05%wt. additives.

Growing demand of biodegradable cutting fluids enhances the application of vegetable based MQL which may be an alternative to conventional cooling/lubrication. Vegetable oils provide better lubricant film layer due to its triglycerides structure. It also reduces frictional coefficient and accelerates wear resistance. But the thermal instability and higher cost of vegetable oils are some of the remarkable drawbacks.

3.2.2. MQL Using Solid Lubricants

One of the main limitations of MQL is sudden vaporization of cutting fluids at cutting zone before proper cooling and lubrication which affects highly tribological performances. So, effective cooling and lubrication is required at higher cutting speed, feed and depth of cut. In industrial applications higher productivity with environment friendly cutting fluid in economic way is the main concern. Application of solid lubricants such as MoS₂, WS₂, TiC, TiN, TiB₂, graphite, HBN, boron oxide, PTFE etc. is one of the remarkable improvements of MQL [69]. Many researchers studied the influence of solid lubricants in MQL and analyzed their performance on various machining aspects. Some selective studies of researchers are shown in Table 2 Paturi et al. [70] analyzed surface quality of Inconel 718 under pure MQL and MQL with micron sized WS₂ particles (0.5%wt.) with emulsifier oil in MQL (200ml/hr) at a mixing ratio 20:1 and observed 35% improved surface quality than MQL in turning. The anisotropic layer structure and the presence of transition metal dichalcogenide in WS₂ reduced tool chip contact friction and heat generation which effectively lubricated the

work surface. Gunda et al. [71] performed a comparative analysis among dry, flood cooling, MQL (flow rate 42ml/hr) and high pressurized (0.6MPa) solid assisted MQL (flow rate 60ml/hr). This high pressure helps to penetrate cutting fluid in the closest zone of tool/workpiece and tool/chip interfaces. Solid lubricants formed a thin lubrication film layer at higher temperature and flow of solid lubricants at cutting zone reduced plastic contact between tool and workpiece. As a result better surface and less tool wear with higher tool life (34min) was achieved in high pressurized solid assisted MQL at 100m/min cutting speed turning. High pressurized cutting fluid also improves chips breakability. Marques et al. [72] applied two types of solid lubricants 20% (MoS₂, graphite) with vegetable oil LB2000 in MQL (0.5MPa pressure and 40ml/hr flow rate) for turning Inconel 718 at higher cutting speed 250m/min and concluded that MoS₂ solid particles assisted MQL would be better lubrication than graphite solid particles assisted MQL. In reality, for both solid lubricants

reduction of flank wear, surface roughness and no residual stress was found due to lamellar structure of graphite and MoS₂. Sterle et al. [73] measured coefficient of friction between AISI 1045 and uncoated carbide tool pair using an open tribometer. Different cooling techniques were applied and compared based on coefficient of friction at different cutting speeds (50, 100, 150, 150, 200m/min). More robust result was found for MQL with solid lubricants (10µm sized, particles suspended into isopropyl alcohol flow rate 200ml/hr).

From review analysis it is clear that solid lubricants help to reduce friction between interfaces, improve tool life through reducing tool wear, increase material removal rate, productivity, and enhance the quality of final product. High cost, apply and disposal complexity limit the use of solid lubricants to specific machining processes. More studies are needed for improving the performance of solid lubricants.

Table 2. Summary of published research works on Minimum Quantity Lubrication (MQL) using solid lubricants.

Findings	35% reduction of surface roughness is achieved in solid particles assisted MQL.	Solid lubricants reduce tool wear and surface roughness than wet, dry and MQL.	Vegetable oil with graphite particles improves lubrication quality and reduces surface roughness but higher wear rate is due to lack of oxygen. MQL with MoS ₂ solid particles may be considered as an alternative to dry turning.	Solid lubricants reduce tool wear and surface roughness than wet, dry and MQL.
Machining Environment	MQL, solid lubricant assisted MQL	High Pressure Minimum Quantity Solid Lubricant cooling	MQL, solid lubricant assisted MQL	Dry, wet, cryogenic cooling, MQL with cryogenic, MQL with solid lubricants
Machining Process	Turning	Turning	Turning	Sliding
Coolant types	Emulsifier oil based cutting fluid, WS2 solid particles	20% MoS ₂ with SAE oil	Vegetable based oil with graphite (25-27µm) and MoS ₂ (5-7µm)	MoS ₂
Used materials	Inconel 718	Mold steel	Inconel 718	AISI 1045
Authors	Paturi et al.(2016)	Gunda et al.(2016)	Marques et al.(2019)	Sterle et al.(2018)

3.2.3. MQL Using Nanofluids

In case of high speed machining conventional fluids perform as better lubricants but their poor thermal properties restrict their use [74]. To overcome this problem nanometer sized particles are used as additives with conventional cutting fluids [75]. Suspending nanoparticles in base oils enhance the properties of cutting fluids such as viscosity, wettability, heat conductivity and convectivity [76].

This newer cutting fluid provides better thermal properties and creates better chemical tribofilm between interfaces of tool and workpieces that enhances the anti-friction or anti-wear performances. Some published research works on nanofluids are selected in random and listed in Table 3 Uysal et al. [77] conducted experiments in milling of martensitic stainless steel under pressurized air mist with MoS₂ nanoparticles at different flow rates. The experimental results proved that MQL with MoS₂ nanoparticles enhances the reduction of initial tool wear than MQL without nanoparticles and higher flow rate of air mist provides better results in all MQL. Proper selection of nanoparticles is an important issue. Rabiei et al. [78] investigated the properties of six types water based nano cutting fluids. TiO₂, SiO₂ and Al₂O₃ are efficient

as lubricants and CuO, NiO, Multi-walled carbon nano tube (MWCNT) are suitable as coolants. Al₂O₃ was found the best nano lubricant among these six types for grinding 52100 hardened steel. Minimum grinding force and grinding temperature were achieved for Al₂O₃ nanoparticle assisted MQL. Wang et al. [79] analyzed the effect of workpiece material and nanofluid types on grinding performances. The results revealed that Al₂O₃ nanofluid is suitable for hard material Inconel 718 and MoS₂ is better for soft carbon steel AISI 1045. Eltaggaz et al. [80] performed a comparative analysis between pure MQL and MQL with nanofluids. In experiments 0.4%wt. Al₂O₃ gamma nano particles were added with vegetable oil. These nanofluids provided better thermal conductivity and lubrication properties than pure base oil and flank wear rate was also reduced in nanofluid based MQL. Gutnichenko et al. [81] added graphite nanoparticles (~30nm, 0.2% vol.) with rapeseed vegetable oil in turning alloy 718. This modified vegetable oil increased the efficiency of MQL in terms of process stability, surface quality, cutting force and tool wear. Sustainability assessment is a qualitative optimization tool for assessing the sustainability indices of experimental trials. Hegab et al. [82] performed MQL with additives at different weight percentages and without additives

for assessing sustainability based on power consumption, surface quality, personnel health, safety and environmental effect in turning Inconel 718 alloy. Slight differences are found between experimental optimum results and sustainable optimum parameters.

Better lubrication and heat dissipation qualities may be enhanced by using hybrid nanofluids. Zhang *et al.* [83] analyzed the effect of different sized (70, 50, 30 nm) nano-particles (2% vol.) for grinding Inconel 718. Mixing of 30nm sized Al_2O_3 with 70nm sized SiC provided better surface quality than other mixing ratios. Zhang *et al.* [84] studied the effect of pure nanoparticles (pure MoS₂, pure CNT) and mixture of two or more nanoparticles (MoS₂/CNT) with different mixing ratio (1:1, 1:2, 1:3, 2:1). Due to synergistic effect 6%wt. hybrid nanoparticles MoS₂/CNT with mixing ratio (2:1) provided minimum surface roughness and coefficient of friction. Normally tool wear progresses highly at the initial stage of machining that has a detrimental effect on

the process. Sharma *et al.* [74] mixed graphene and alumina at volume concentration ratio (10:90) and tested for different volume concentration of nanoparticles. Hybrid alumina graphene nanoparticles reduce cutting temperature, improve surface integrity and also minimize tool wear. Lv *et al.* [85] investigated machining and tribological characteristics of MQL in milling process using hybrid (graphene oxide (GO)/silicon dioxide (SiO₂)) nanofluids in different concentration. After investigation mixing concentrations of 0.02% wt. GO and 0.5% wt. SiO₂ with vegetable oil provided best lubrication with minimum worn scar diameter and coefficient of friction. In another research (Rabiei *et al.* [86] achieved 27.3% reduction of friction coefficient for hybrid Al_2O_3 / multi-walled carbon nano tube (MWCNT) nanofluids in grinding of 100Cr6 hardened steel. It is clear from review that nanofluids improve machining performance significantly but more studies are needed for finding the optimum size of nanoparticles and its concentration ratio in base oil.

Table 3. Summary of published research works on Minimum Quantity Lubrication (MQL) using nanofluids.

Findings	MQL with nanofluid improves heat dissipation and tool life.	Higher percent nano additives increase tool wear due more internal colloidal collision. 2% weight MWCNT and Al_2O_3 provides better results.	Smaller size of Al_2O_3 provides better surface quality but material removal rate is increased for larger sized Al_2O_3 nanoparticles mixing with SiC.	Pure Molybdenum disulphide provides better lubrication than pure carbon nano tube. Molybdenum disulphide / carbon nano tube provides better lubrication due to synergistic effect.	Nanoparticle assisted MQL with 40ml/h flow rate reduced wear by 19.9% and surface roughness by 22.5%	Hybrid nano particles generate less tool wear and surface roughness than pure alumina nanoparticles.	Worn scar diameter is reduced and improved surface is achieved through using nanofluids.
Machining Environment	MQL, MQL with NFs	MQL with NFs	MQL with NFs	MQL with NFs	Dry, MQL, MQL with NFs	MQL with NFs	MQL with hybrid NFs
Machining Process	Turning	Turning	Grinding	Grinding	Milling	Turning	Milling
Used Nanoparticles	Al_2O_3	MWCNT/ Al_2O_3	Al_2O_3 /SiC	MoS ₂	MoS ₂	Grapheme nanoplatelets with alumina	Graphene oxide/Silicon dioxide hybrid nanoparticles
Used materials	ADI	Inconel 718	Inconel 718	GH4169 Ni based alloy	AISI 420	AISI 304 steel	Ti6Al4V
Authors	Eltaggaz <i>et al.</i> (2018)	Hegab <i>et al.</i> (2018)	Zhang <i>et al.</i> (2017)	Zhang <i>et al.</i> (2015)	Uysal <i>et al.</i> (2015)	Sharma <i>et al.</i> (2018)	Lv <i>et al.</i> (2018)

3.2.4. MQL Using Ionic Liquids (ILs)

In recent years it is tried to innovate newer types cutting fluid and MQL with ionic liquids is one of the newer innovative approaches. Ionic liquids are normally liquid salts (<100°C temperature) and consist of organic cation and inorganic anion. Like other additives ionic liquids are mixed with base oil at various ratios for enhancing the properties of base oil. Several researchers have already studied the performance of ionic liquids as an additive of cutting fluids and some of them are discussed in Table 4. Davis *et al.* [87] studied ionic liquids as additive with minimum quantity lubrication for titanium machining and also compared with dry machining and water based MQL (MQL with H₂O). Ionic liquid was prepared by adding 0.5%wt. BMIM-PF₆ with deionized water in experiments. In this study 60% tool wear

improvement, 15% lower force in tangential and radial directions was achieved. In another research, Goindi *et al.* [88] machined AISI 1045 using 1% wt. three different types ionic liquids BMIM-PF₆, BMIM-BF₄, BMIM-TFSI individually with vegetable oil and better tribological properties were achieved than dry cutting, dry cutting with compressed air and MQL with vegetable oil. Pham *et al.* [89] evaluated the process capability and sustainability of ionic liquid. Two types of ionic liquids: EMIM-TFSI and BMIM-I were compared with dry milling, other conventional cutting oils cooling and distilled water cooling. In this experiment BMIM-I provided better surface integrity than others. Sani *et al.* [90] tested the performance of ammonium based (AIL) and phosphonium based (PIL) ionic liquids with modified jatropha oil (MJO) in machining of AISI 1045 under MQL environment and

observed that a small quantity of ionic liquids enhances the machining performance highly. The better results were obtained from MJO+ 10%AIL and MJO+1%PIL cutting fluids. Now it can be concluded that ionic liquids enhance the tool wear resistance through tribo-chemical reactions between

ionic liquids lubricants and workpiece/tool surface. This lubricant acts as an additive to form a tribo-layer for reducing tool wear and coefficient of friction. Application of ionic liquids as neat lubricants or additives of different base oils is a newer technique of cooling so more detail study is needed.

Table 4. Summary of published research works on Minimum Quantity Lubrication (MQL) using ionic liquids.

Findings	Tool wear is reduced by 60% in MQL with ILs than dry cutting and 15% than MQL.	A minute quantity of ionic liquids significantly affects the tribology of machining process.	BMIM-I ionic liquid shows less volatility and provides better surface.	MJO+10%AIL and MJO+PIL provide better performance than synthetic ester.
Machining Environment	Dry, MQL with water and MQL with ILs	Dry, MQL, MQL with ILs and flood cooling	Dry, Flood cooling and MQL with ILs	MQL, MQL with ILs
Machining Process	Turning	Turning	End milling	Turning
Coolant types	BMIM-PF6 with water	Vegetable oil with BMIM-PF6, BMIM-TF4, BMIM-BFTS	EMIM-BFTS, BMIM-I	Modified Jatropha oil (MJO) with Ammonium based (AIL) and Phosphonium based (PIL) ionic liquids, synthetic ester
Used materials	Titanium	AISI 1045	Al-5052	AISI 1045
Authors	Davis et al. (2015)	Goindi et al. (2015)	Pham et al. (2014)	Sani et al. (2019)

3.2.5. Some Other New Features of MQL

Some other newer techniques such as Contact Charged Electrostatic Spray Lubrication (CCESL) [91], variable time controlled pulse [92], Electrostatic Minimum Quantity Lubrication (EMQL) [93], Ranque Hilsch Vortex Tube (RHVT) in Nitrogen gas assisted MQL (RHVT-NGMQL) [94] are also experimented for enhancing cooling/lubrication.

3.3. Cryogenic Cooling

Cryogenic cooling is another alternative sustainable cooling technique. In cryogenic cooling Liquid Nitrogen (LN₂) at -196°C, carbon dioxide (CO₂) or dry ice at -78.5°C are used as coolant in cryogenic cooling process. These coolants easily evaporate to atmosphere without any harmful effects. In recent years, effective cooling with clean environment makes this technique popular. Some limitations of cryogenic cooling are - the cost of cryogen is high and the performance highly depends on the reliable supply of cryogen. Another important limitation is this technique is better for cooling but not for lubrication.

Based on cryogen type cryogenic cooling has two operating methods-cryogenic cooling with liquid nitrogen (LN₂) and cryogenic cooling with dry ice or CO₂ (-78.5°C).

3.3.1. Cryogenic Cooling with Liquid Nitrogen (LN₂)

Since 1950s liquid nitrogen (LN₂) was used as a cryogenic coolant but now its use is increasing rapidly because of its easily evaporation characteristic in nature (79% of air is nitrogen) and environment friendliness.

Researchers have been performing many research works on various aspects of cryogenic cooling using liquid nitrogen in different machining processes. Dhar et al. [95-96] experimentally proved that cryogenic cooling by liquid nitrogen jet reduced more chip-tool interface temperature, surface roughness and tool wear for different materials machining than dry machining. Fredj et al. [97] used cryogenic cooling for ground surface improvement of AISI 304 steel. In cryogenic cooling 40% reduction of surface

roughness, better resistance to stress corrosion and pitting corrosion, higher level of work hardening were achieved. Umbrello et al. [98] investigated the effect of cryogenic cooling on the surface integrity of hardened AISI 52100 steel. Research results showed that better surface roughness, finer grain size, reduced white layer regions were achieved in cryogenic cooling than dry machining. Manimaran and Pradeepkumar [99] performed a comparative analysis among dry, wet and cryogenic cooling. The analysis concluded that specific energy, grinding force and surface roughness were reduced satisfactorily in cryogenic cooling than dry and wet. Another remarkable result was that, increasing pressure of cryogen improves surface quality 12% in cryogenic grinding for this wheel work-piece pair. Dinesh et al. [100] conducted turning experiment on AZ60 magnesium alloy under various cutting parameters and investigated the positive influence of cryogenic cooling on surface integrity, hardness, cutting temperature and cutting force. Shokrani et al. [101] employed cryogenic cooling for cobalt chromium alloy machining and found 71% reduced surface roughness with 96% improvement of tool life than conventional cooling. Cryogenic cooling is also proved as better cooling process for hard machining. Chip morphology has an impact on machining performance because long, highly curled chips deteriorate surface quality. Aramcharoen [102] investigated the influence of cryogenic cooling on tool wear and chip morphology in turning titanium alloy. Using conventional cooling at 100 m/min cutting speed built up edge was generated after 3min turning but within this range of time no built up edge was found in cryogenic cooling. Scanning Electron Microscope (SEM) analysis results showed that helical chips were produced in cryogenic cooling turning but in conventional oil cooling most snarled chips were produced which are highly undesirable. Yousefi et al. [103] focused on the influence of coated tools in cryogenic cooling. 2µm thick CrN coating provided better results for roughness 0.8µm but unable to prevent adhesion to titanium work material. Isakson et al. [104] agreed with previous other researchers that cryogenic cooling may be applied instead of

flood cooling without sacrificing surface integrity of titanium alloy.

Mia [105] carried out milling of AISI 1060 steel using HSS insert instead of carbide insert using internal cryogenic cooling. ANOVA results revealed that surface roughness, cutting force and specific cutting energy are highly influenced by cooling followed by feed rate and lastly cutting speed. Internal cryogenic cooling with cutting speed 26m/min and feed rate 58mm/min provided optimum experimental results. Nie *et al.* [106] performed hard machining of AISI 52100 steel under dry environment and cryogenic cooling. In dry environment white layer formation is drastically increased at higher cutting speed but in cryogenic cooling white layer formation is almost same in varying cutting speeds Mia *et al.* [107] conducted turning operation of Titanium alloy under dry condition and cryogenic cooling with mono jet and dual jet of liquid nitrogen. In that research, life cycle assessment of cryogenic cooling was performed and the observed result pointed out that the cooling technique has a direct relationship with environmental aspects. In another research, Sivaiah and Chakradhar [108] applied MQL and cryogenic cooling in turning 17-4PH stainless steel for comparative analysis based on tool wear and surface roughness. Cryogenic cooling with liquid nitrogen provided less tool wear and surface roughness and researchers concluded the cryogenic cooling as a clean technique because liquid nitrogen easily evaporates after penetration that agreed with previous described review results. Dhananchezian [109] studied the mechanical characteristics of difficult to cut metal Ni based Hastelloy C-276 under cryogenic cooling and dry turning. This cooling technique reduced cutting zone temperature 61~68%, cutting force and surface roughness by 8-33% than dry turning. Cutting tool performance was also improved through controlling the wear mechanism.

Researchers also discussed some negative results of cryogenic cooling in machining processes. NALBANT and YILDIZ [110] reported cryogenic machining as a poor cooling method for milling AISI 304 steel based on their experimental results. Cutting force, torque is higher in cryogenic cooling than dry technique for used work-piece tool pair in experiments. It is also found that if cutting speed is lower than 200m/min then chattering occurs in cryogenic cooling. It can be pointed out that better performance of cryogenic cooling depends on tool/workpiece pair. Cryogenic cooling using liquid nitrogen enhances rapid cooling, reduces built up edge, abrasive and chemical wear highly. Besides that cryogenic cooling is highly clean and environment friendly cooling technique.

3.3.2. Cryogenic Cooling with Dry Ice or CO₂ Snow

Applying CO₂ flow in liquid form is another technique of cryogenic cooling. Murugappan *et al.* [111] implemented precooling cryogenic using dry ice and two different types cutting inserts in turning Al 6063. The experimental results showed that insert type and cooling techniques have influential effect on productivity and product quality. Biermann and Hartmann [112] used CO₂ cryogenic process

cooling for reducing burr formation in drilling of quenched steel 34CrNiMo6 and aluminum alloy AlMgSi1. Cordes *et al.* [113] performed cryogenic CO₂ cooling in which the flank wear was reduced by 63%, cutting temperature was reduced by 55% and material removal rate was increased by 72% than dry milling at cutting speed 320m/min. Rahim *et al.* [114] carried out experiment on orthogonal cutting process of AISI 1045 under MQL and super critical CO₂ cooling. It was found that super critical CO₂ cooling is more efficient for reducing cutting force, tool chip contact length, specific energy, chip thickness and cutting temperature than MQL. Finally, it can be noted that cryogenic (CO₂) cooling reduces burr formation, minimizes tool wear with uniform wear length, removes white layer formation and improves tool life.

3.4. Hybrid Cooling/Lubrication Techniques

Researchers are now aiming to combine two or more cooling strategies for attaining the better synergistic effects of cooling techniques in cutting processes. Pereira *et al.* [115] proposed new nozzle adapter for combining the effect of MQL and cryogenic CO₂ (-80°C). This new method achieved 93.5% efficiency of conventional cooling for increasing tool life. Park *et al.* [116] applied cryogenic cooling (using liquid nitrogen) with MQL using exfoliated graphite nano particles with vegetable oil as base oil for machining titanium alloy and found that this hybrid cooling reduced cutting force and tool wear than conventional cooling. Hybrid cooling (cryogenic cooling with MQL) is considered as a promising alternative to conventional cooling but some research results revealed that the hybrid cooling may be an alternative to MQL not to conventional cooling. Hanenkamp *et al.* [117] combined CO₂ (-78.5°C) cryogenic internal cooling with MQL for investigating surface roughness and tool wear in drilling of Ti6Al4V alloy using a rotating tool 50CrMo4. This hybrid cooling reduced 64.5% surface roughness than MQL but increased 11% than conventional cooling. Not only that hybrid cooling (cryogenic CO₂ with MQL) also provided finer surface zone with no crack and white layer formation and tool wear was also minimized. Iturbe *et al.* [118] performed turning operation of Inconel 718 for 8-20minutes under dry, conventional cooling and (cryogenic cooling (LN₂) + MQL). Results revealed that almost four times larger surface damage was found in hybrid cooling due to higher flank wear rate than conventional cooling. The authors concluded that surface quality depend not only cooling process but also tool flank wear. From the review results it can be concluded that hybrid cooling/lubrication technique is now in the introduction stage and further research studies are needed for improving the performance and robustness of hybrid cooling/lubrication techniques.

4. Conclusions

In this study, first of all, various cooling/lubrication processes and cutting fluids are introduced and then, effect of this cooling/lubrication processes and cutting fluids on cutting parameters such as, tool- workpiece temperature, cutting forces, surface roughness, tool wear are reviewed. Present analysis shows that not only cooling/lubrication processes

influence on machining parameters but also type of base fluid and additives, size of additive particles and concentration of additives in base fluid are important too. Review results have shown that dry cutting is environmentally safer, most sustainable and less costly than cutting process with coolants/lubricants but dry cutting is not suitable for cutting processes with higher heat generations. So, further research is needed to remove these limitations of dry cutting. Positive and negative effects of all presently practiced cooling/lubrication strategies are listed in Table 5. To eliminate the bad impacts of conventional cooling methods such as flood cooling, mist cooling and HPC, researchers have tried to apply MQL with different types less toxic and biodegradable cutting fluids. Elimination of mineral oil and other toxic cutting fluids are successfully done by using vegetable oils, nanofluids, ionic liquids etc. Cryogenic cooling is another alternative to conventional cooling which is green, safer, sustainable and

efficient but initial cost is higher that limits its use.

5. Future Scope of Research

Some points are narrated below for improving cooling/lubrication techniques in future by more research works.

1. Proper selection of coated tools in dry machining of hard to cut metals need to be investigated.
2. Research and development for modifying vegetable oils to overcome its limitations such as low thermal stability and higher oxidation.
3. More and more research is needed for improving the performance of nanofluids through optimizing the size of nanoparticles and mixing ratio into base oils. Hybrid nanofluids are another attractive scope of further research.

Table 5. List of positive and negative impacts of various cooling/lubrication techniques.

	Huge quantity of cutting fluid is applied. Not a clean cooling technique. Responsible for many diseases of workers. Higher cost of cutting fluids.	Mist cooling provides wet cutting environment that makes the working space slippery. Skin diseases may occur.	Higher amount of fluids are needed. Surface roughness may be raised. Recycling cost of cutting fluid is involved. Fluids from chips need to be separated. Cooling environment is not clean. Inhalation problem may occur. Energy consumption is higher.	Poor surface finish and higher tool wear rate is found. Increased cutting temperature. Difficult to machine hard to cut metals. Higher cutting force is found so specific energy requirement is higher.	Cheap breakability is poor. Inhalation problem may occur through MQL spray. Proper cooling is not achieved. Not suitable for grinding process.
Positive impacts	Highly applicable for energy extensive processes such as grinding.	Cheap cooling process. Cooling ability is higher. Reduces cutting temperature. Environmental friendliness is higher than flood cooling.	Tool life is increased highly. Cooling rate is higher. Easy chip breakability. Cutting force is reduced. Suitable for hard to cut metals machining.	No cutting fluid is used so cost is minimum, no risk of operators health. Clean machining is achieved. Easy recycling due to cleanliness of chips.	Less consumption of cutting fluid. So economic and ecological impact is minimized. Specific energy requirement is minimized. Improved surface quality and more sustainable technique. Clean and green process.
cooling/lubrication processes	Flood cooling	Mist cooling	HPC	Dry machining	MQL

Table 5. Continued.

Negative Impacts	CO ₂ is responsible for global warming. Set up and tooling cost, price of cryogen are higher.	Equipment cost is higher and set up is complex than other cooling/lubrication.	Costs of vegetable oil are comparatively higher than conventional fluids. Oils must be separated from chips.	Without addition of any coolant its cooling performance is poor. Production process is costly	Higher cost of nanoparticles.	Synthesis of ionic liquids as neat lubricants or additives with base oil is a complex process. ILS are costly.
Positive impacts	Clean and environment friendly cooling process with lubrication through forming a gas layer between interfaces. Completely harmless to operators health. Improves surface quality, reduces tool wear and cutting temperature rapidly. It also improves chip breakability.	Cooling and lubrication efficiency is expected be higher.	Nontoxic, biodegradable and environment friendly technique. Better cooling and lubrication. Improved tool life with less tool wear can be achieved.	Improves tool life, reduces shear angle and tool chip contact length. Improves surface roughness. Reduces tool chip interaction through forming tribofilm between interfaces.	Deep penetration of nanofluids can be achieved. So temperature at the cutting zone is highly minimum.	Tool wear and coefficient of friction is highly reduced. Ionic liquids is recyclable and in most cases biodegradable.
Name of cooling/lubrication techniques	Cryogenic cooling	Hybrid cooling/lubrication	Vegetable based oils	Solid Lubricants	Nanofluids	Ionic liquids

Nomenclature

Table 6. Used short terms with proper abbreviations.

WOMS	Water in Oil Mist Spray
HPC	High Pressure Cooling
MQL	Minimum Quantity Lubrication
MQCL	Minimum Quantity Cooling Lubrication
SQL	Small Quantity Lubrication
PVD	Physical Vapor Deposition
NDM	Near Dry Machining
VO	Vegetable oil
NFs	Nanofluids
CNT	Carbon nano tube
MWCNT	Multi walled Carbon nano tube
hBN	hexagonal Boron Nitride
SCCO ₂	Super Critical Carbon-di-oxide
LN ₂	Liquid Nitrogen
NiO	Nickel oxide
SiO ₂	Silicon dioxide
UAG	Ultrasonic Assisted Grinding
ILs	Ionic Liquids
BMIM-PF6	1-methyl 3-butylimidazolium hexafluorophosphate
AIL	Ammonium based ionic liquid
GO	Graphene Oxide
SiO ₂	Silicon dioxide
MoS ₂	Molybdenum disulfide
WS ₂	Tungsten sulfide
CVD	Chemical Vapor Deposition
TiC	Titanium carbide
TiN	Titanium Nitride
TiB ₂	Titanium diboride
PTFE	Polytetrafluoroethylene
Al ₂ O ₃	Aluminum oxide
CaF ₂	Calcium fluoride
CuO	Copper oxide
SiC	Silicon carbide
BMIM-BF ₄	1-methyl 3-butylimidazolium tetrafluoroborate
BMIM-TFSI	1-methyl 3-butylimidazolium trifluoromethyl-sulfonyl imide
EMIM- TFSI	1-ethyl 3-methylimidazolium trifluoromethyl-sulfonyl imide
BMIM-I	1-methyl 3-butylimidazolium-iodide
EG	Ethylene glycol
PEG	Polyethylene glycol

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