



Treatment of Hazardous Solid Waste Using Solidification and Stabilization Technique

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Abstract: The immobilization of toxic metals present in the pharmaceutical effluent treatment plant (ETP) sludge is studied using the solidification/stabilization (S/S) technique. Different mixtures of cement, lime and bentonite as binders and additives (Pulverized fuel ash (PFA), silica fume and quarry dust) are used in order to reduce the mobility of the metal constituent of the pharma sludge as well as to strengthen brick. The interaction between the S/S matrix were studied using X-ray diffraction spectroscopy (XRD), Fourier Transform Infrared Spectroscopy (FT-IR), Thermo gravimetric-Differential Thermal Analysis (TG- DTA), Unconfined Compression Strength, Toxicity characteristics leaching procedure (TCLP) tests. The results showed that the optimized composition matrix have a strong fixing capacity for heavy metal includes Cu, Zn, Fe, Co, Pb, Ni and Cd. All the specimens have been observed to be sufficient in achieving the target compressive strength of 0.3 N/mm² required for landfill disposal and mixed binders (Cement, Lime, and Bentonite) brick can be recommended for external use in construction i.e. for pave of pedestrian roads.

Keywords: Solidification and Stabilization, Pharmaceutical Sludge, Binder, Hazardous Waste, Brick, Compressive Strength

1. Introduction

Growth of population, increasing urbanization and rising standards of living due to technological innovations have contributed to an increase in the quantity of solid wastes generated by industrial, mining, domestic and agricultural activities. These wastes need to be managed properly to minimize their harmful effect on human health and environment. The development in technologies for recycling and reusing waste is critical to the success of current policies on hazardous waste management [1].

This hazardous waste might pose potential effect to human health and healthy environment due to its instability [2]. These can be potentially stabilized using solidification/stabilization (s/s) method which not only alleviates disposal problems but also has economic, ecological and energy saving advantages [3 and 4].

Additives such as cement, clay, slogs, coal fly ash and lime are in s/s technology to immobilize waste continents [1 and 5]. The stabilization process using cement relies on the formation of calcium silicate hydrate ($\text{CaO} \cdot \text{SiO}_2 \cdot n\text{H}_2\text{O}$, briefed as C-S-H), ettringite hydrate ($3 \text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot 3 \text{CaSO}_4 \cdot 32 \text{H}_2\text{O}$) and Monosulphate ($3 \text{CaO} \cdot \text{Al}_2\text{O}_3 \cdot \text{CaSO}_4 \cdot 12 \text{H}_2\text{O}$) in the matrix, due to the hydration reaction of portland cement. Thus, the heavy metals get chemically fixed in the lattice of hydration production as well as physically encapsulated in the matrix. In organic salts, calcium chloride is often used as accelerating additive thus guaranteeing the stabilization and solidification of the sludge [1 and 6].

Indian Pharma industry is became an essential part of modern society and waste production has been an inevitable outcome of the developmental activities [1 and 3]. In the present study the application of sludge derived from waste water pollutant coagulation (ETP sludge) from pharma

industry into unfired bricks has been studied, which further reduces the natural resource degradation. In addition to unconfined compressive strength (UCS) measurements, leaching test, X-ray diffraction (XRD), Fourier Transform Infrared Spectroscopy (FTIR) and Thermo Gravimetric - Differential Thermal Analysis (TG-DTA) have been investigated the solidification mechanism of the bricks.

2. Materials and Method

The materials used in this study have been given in table 1.

Table 1. Reactant materials used for study.

S. No	Material	Purpose of use	Characteristic
1	Pharmaceutical industry waste	Needed to treat	Hazardous
2	Cement	Binder	Construction Compound
3	Lime	Binder	Coagulant Compound
4	Pulverized fuel ash	CO- Binder	Hazardous
5	Bentonite	Binder	Coagulant Compound
6	Silica Fume	strength increaser	Hazardous
7	Quarry dust	strength increase	Hazardous

The initial characteristic of the sludge sample has been given table 2.

Table 2. Physico-chemical characterization of ETP sludge.

S. No	Parameter	Results
1	Color	Ash Color
2	State	Semi solid
3	pH	8.5

Table 3. Composition of S/S Matrixes.

COMPOUNDS	COMPOSITION						
	SERIES A			SERIES B			SERIES C
	TYPE I	TYPE II	TYPE III	TYPE I	TYPE II	TYPE III	
Nomenclature of The Bricks	AC 1	AB 1	AC 1	BLB 1	BBC 1	BLC 1	CLBC 1
SLUDGE (%)	10	10	10	10	10	10	10
PULVERISED FUEL ASH (%)	35	35	35	35	35	35	30
LIME (%)	30	-	-	15	-	15	10
BENTONITE (%)	-	30	-	15	15	-	10
CEMENT (%)	-	-	30	-	15	15	10
SILICA FUME (%)	20	20	20	20	20	20	20
QUARRY DUST (%)	5	5	5	5	5	5	10
TOTAL (%)	100	100	100	100	100	100	100

2.2. Analytical Techniques

2.2.1. X-ray Diffraction (XRD)

The crystalline structure of the brick, which affords better understanding on the reaction products, is analyzed by X-ray diffraction (XRD). XRD scans of brick material is performed with Bruker D 8 advanced X-ray diffractometer operated at 40 kV and 30 mA (CuK- α radiation ($\lambda=1.5418 \text{ \AA}$)) in the range 20–80° 2 θ at scanning rate of 1° 2 θ per minute.

2.2.2. Fourier Transform Infrared Spectroscopy (FTIR)

Infrared spectra analysis is made using Perkin Elmer FTIR

S. No	Parameter	Results
4	Moisture content (%)	12%
5	Density (g/cm ³)	0.6451
6	Specific gravity	0.635
7	Organic matter	14%
8	Zn (mg/Kg)	131.2
9	Fe (mg/Kg)	2012.1
10	Ni (mg/Kg)	80.8
11	Co (mg/Kg)	12.7
12	Pb (mg/Kg)	37.7
13	Cd (mg/Kg)	3
14	Cu (mg/Kg)	282.7

2.1. Methodology

The unfired bricks have been prepared in duplicates using 3 binders (cement, lime and bentonite). The ETP sludge has been dried in a hot air oven for 24 h at 105°C and ground to less than 9.5 mm in size to aid workability of the sludge-ash-binder mixture during casting. The PFA and binder are mixed in a small container, after 5 min it is blended with water. The dried sludge is added to blended mixer. After fine mix, the industrial by-products silica fume and quarry dust are added to develop the strength of the brick.

This unfired bricks from waste are fabricated in wooden moulds with internal dimensions of 120 mm X 65 mm X 30 mm. The moulds are filled with above prepared admixes and kept in moist condition for 24h. At the end of this period the bricks are removed from the moulds and cured in air at room temperature for 28 days. The structural, functional groups, thermal behaviour, heavy metal leachability and strength of the s/s matrixes have been carried to evaluate the workability of s/s process. The composition of the bricketing materials are reported in table 3.

spectrometer [7, 8] using KBr method. Wave length number ranges from 4000-400 cm⁻¹. Pellet making has been done using hydraulic pump manufactured by Kimaya Engineers.

2.2.3. Thermo Gravimetric Differential Thermal Analysis (TG-DTA)

The thermal behavior and weight loss of the sample is determined using TG-DTA. TG-DTA of the sample has been done by S-II EXSTAR-6000, TG/DTA-6300 thermal analyzer. Sample loaded in aluminum container and heated to 800°C at the rate of 2 K/min with air circulating at a speed of 150 ml/min.

2.2.4. Toxicity Characteristic Leaching Procedure (TCLP)

Toxicity Characteristic Leaching Procedure (TCLP) of S/S sludge bricks (waste create bricks) has been conducted as per the standard procedures described by USEPA 1996 (8). The heavy metals are analyzed by Atomic Absorption Spectrometer (AAS).

2.2.5. Unconfined Compression Strength (UCS)

UCS of unfired cubes are measured by compression testing machine as per BIS specification code (IS 4031) (IS: 1077-1992).

3. Results and Discussion



Figure 1. Bricks Prepared by solidification and stabilization of wastes.

Where AL 1 - lime binder brick; AB 1- bentonite binder brick; AC 1- cement binder brick; BLB 1- bentonite and lime mixed binder brick; BBC 1- bentonite and cement mixed binder brick; BLC 1- lime and cement mixed binder brick; CLBC 1- cement, lime and bentonite mixed binder brick.

The fig 1 shows the s/s matrixes, prepared using pharma ETP sludge with different binders and additives. The detailed

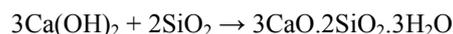
results and discussion are presented as follows.

3.1. Reaction Product Identification by XRD in the Brick Matrix

X-ray diffraction (XRD) pattern showed the crystalline structure of the brick, which affords better understanding on the reaction products. AL 1, AB 1, AC 1, BLB 1, BBC 1, BLC 1 and CLBC 1 bricks diffractograms have been observed to shown similar compounds like portlandite, gypsum, ettringite, alite, belite, quartz and calcite peaks (fig-2). Only the ettringite peak has not observed in AB 1. The intensities of gypsum reflection peaks have stronger intense than that of portlandite in AL 1, AB 1, AC 1, BLB 1, BBC 1 bricks, while compared to BLC 1 and CLBC 1 bricks.

In CLBC 1 matrix it has been observed that the intensity of calcite is weaker than ettringite reflection peak.

Portlandite resulted from cement hydration which can react with silica in the sludge to form C-S-H gel (pozzolanic reactions). This can be further elucidated by the following equations:



Tricalcium and Dicalcium silicates in portland cement reacted concurrently with water and produced strength enhancing compounds calcium hydroxide (portlandite) and ettringite (E).

Ettringite has been formed via the reaction of calcium and alumina in lime or cement with sulphate present in sludge, it favoured the compressive strength. The presence of calcite is attributed by the carbonation of sample during drying and preparations [9].

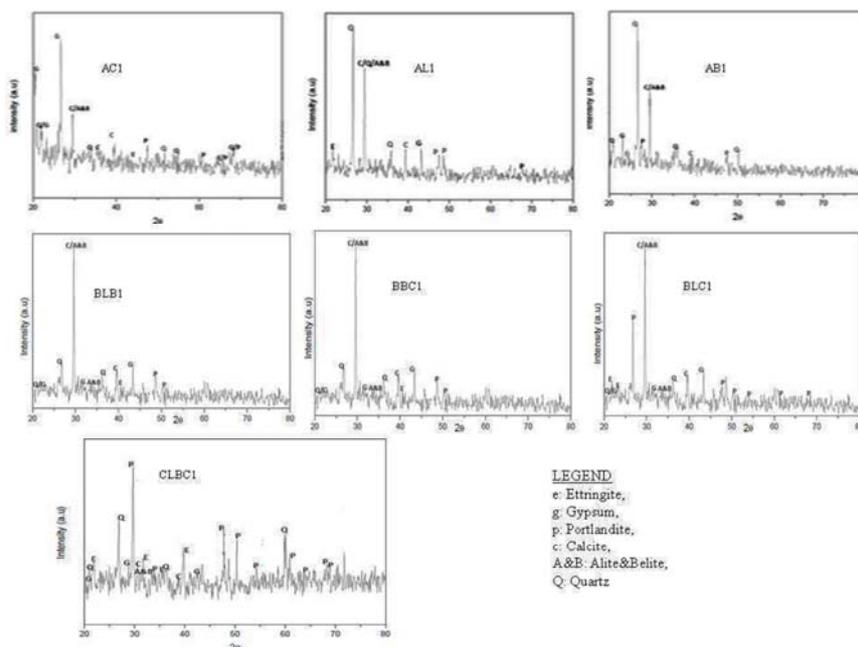


Figure 2. XRD pattern of the brick matrix.

3.2. Functional Groups Analysis by FT-IR

FTIR analysis of the dried unfired bricks has been carried in the frequency ranged between 400 and 4000 cm^{-1} . The IR spectra results of AC 1, AL 1, AB 1, BLC 1, BLB 1, BBC 1 and CLBC 1 geo-polymer matrixes had shown in fig-3. The considerable broad bands located at 3200–1700 cm^{-1} are assigned to O-H stretching and H-O-H bending respectively [10]. The intense peaks at about 875.57 and 712 cm^{-1} are attributed to the metal species with O-H bonding in all the unfired brick samples. O-H stretching band centered at 3424.35 cm^{-1} , 3435 cm^{-1} , 3417 cm^{-1} corresponding to the bound water molecules in the AL 1, AB 1 and BLB 1 bricks. A

strong band around 1402 cm^{-1} -1428 cm^{-1} is assigned to calcite present in the Bi-binder bricks (BBC 1, BLB 1 and BLC 1) matrix. Ettringite has been observed around 1106 cm^{-1} in all unfired brick matrixes. Except AB1 and AC1 matrix, the presence of strong peaks at 874.57 and 783.41 cm^{-1} clearly confirm that the metal contaminants have been effectively stabilized within the ettringite bonds [4 and 11]. Around 1430 cm^{-1} , CH_3 bending has been observed in AB1, AL 1, BBC 1 and CLBC 1 matrixes [12]. Abroad envelope centered at 3440 cm^{-1} has been assigned to -OH stretch of calcium hydroxide in AC 1, BLC 1 and CLBC 1 [13]. Portlandate/Calcite is represented at 1435.62 cm^{-1} in CLBC 1 matrix.

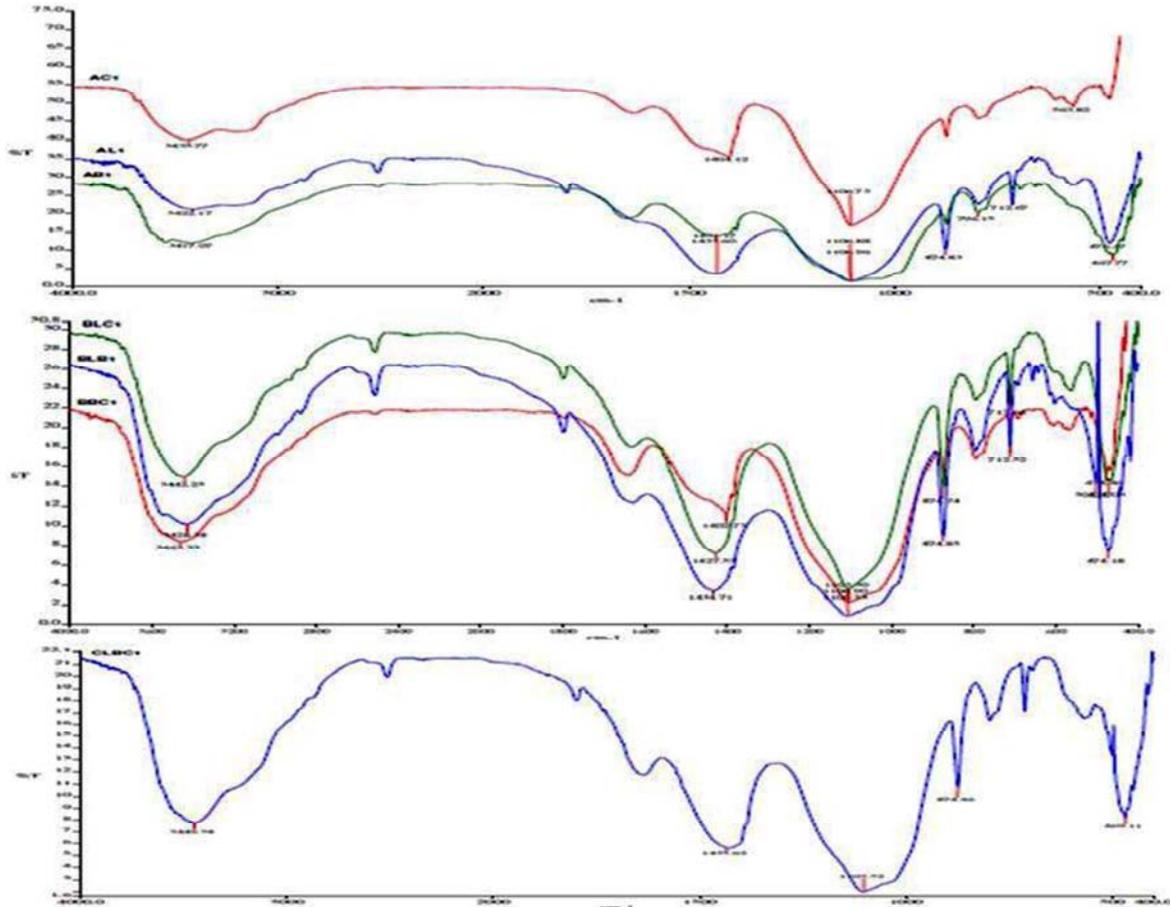


Figure 3. FTIR analysis of the bricks.

3.3. Thermo Gravimetric-Differential Thermal Analysis (TG- DTA)

In thermo gravimetric analysis all the brick samples have been shown weight loss, where the identifiable 3 zones have been observed. The first zone of the mass loss might be attributed to the evaporation of physically and chemically bounded water, second zone of the mass loss is due to the decomposition of the stable hydrates of the calcium aluminates and calcium silicates. Finally the 3rd zone of the mass loss represents the decomposition of the calcium carbonates at 780°C [14]. The Portland dehydration is represented at 470°C -510°C [15 and 16]. Based on the

thermal analysis weight loss of the unfired bricks are in the following order: AC 1> BLB 1> BLC 1> BBC 1> CLBC 1> AL 1> AB 1.

Endothermic peak at 110°C has been observed for AC 1, AB 1, BLB 1 and BLC 1 brick specimens, while the exothermic peak at 500°C has been observed in all the brick matrixes. The endothermic peak around 110°C corresponds to removal of structural water from matrixes [1]. However the exothermic peak at 500°C correspond to dehydroxylation of the portland compounds [1, 6, 16, 25].

In AB 1, BLB 1, BLC 1 and CLBC 1 bricks the exothermal peaks have been observed between 750°C -

810°C, which corresponds to the decomposition of calcite and alite [6, 17].

In CLBC 1 brick, endothermic peak hasn't observed. Such

type of bricks might be usable for heat managing application (furnace) practices, since they do not have heat loss.

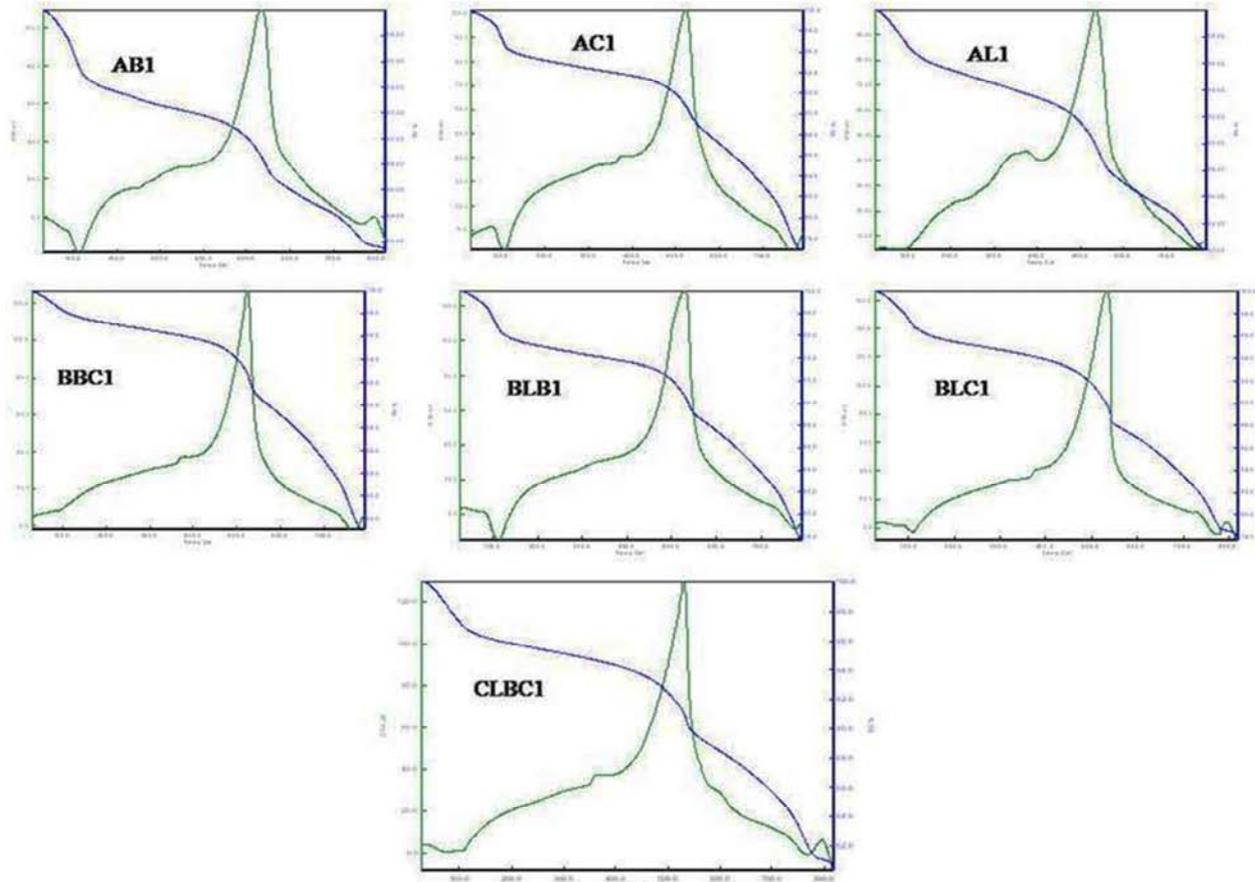


Figure 4. TG DTA analysis of the samples.

3.4. TCLP Leaching Studies

Metal Leaching test has been conducted to investigate the immobilizing ability of S/S formulations [18 and 19]. The variable metal concentrations in the leachate of the different unfired bricks (s/s) have been reported in Table-4. Results from TCLP method shown insignificant levels of heavy metals and comply with the concentration limits set by EPA (2005) [20].

The metals concentrations in the leachate have been observed to be within the acceptable limits. It has been observed that fly ash along with lime, bentonite and cement are very effective in lowering the leaching of heavy metals. Lime, bentonite and cement maintain the sludge at a high pH in the range of 9-11, immobilizing the toxic heavy metals as insoluble hydroxides [19 and 21]. The hydrated cementitious products bind the metals either through chemical or physical bonds. The addition of fly ash with pozzalon material is very effective in lowering the leaching of heavy metals in waste [17, 19 and 21].

The complexes in the sludge might react with the silicate matrix (C-S-H) and C-A-H as long as silicate and aluminates are free available. Chemical gypsum in the sludge reacted with alumina phases to form ettringite, which

contributed to compressive strength as well as restricts the release of the heavy metals from unfired bricks [17, 19]. Under aqueous condition OH ions are released from calcium hydroxide and other forms of hydroxyl compounds present in the bricks contributes alkaline environment, which reduced the release of heavy metals.

Table 4. Concentration of Heavy Metals in Leachate (TCLP).

Bricks	Concentration Level (mg/L)						
	Cu	Zn	Fe	Co	Pb	Ni	Cd
AL 1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
AB 1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
AC 1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
BLB 1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
BBC 1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
BLC 1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
CLBC 1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1

3.5. Evaluation of Physical Engineering Property of the S/S Samples by Compressive Strength

Unconfined compressive strength (UCS) is one of the important parameter, which evaluates the cohesive solidified effect of mixer (waste). After 28 days of the drying [22], the compressive strengths of the solidified sludge bricks are

measured and represented in fig-5. According to the compressive strength analysis the specimens have been observed to be sufficient to achieve the target compressive strength of 0.3 N/mm² required for land fill disposal [6].

The compressive strength of the single binder bricks i.e., AL 1, AB 1 and AC 1 are ranged from 0.30 N/mm² - 4.96 N/mm² and 2.65 N/mm² - 5.45 N/mm² for double binder-sludge bricks i.e., BLB 1, BBC 1, BLC 1 and CLBC 1, where as the compressive strength of CLBC 1 brick is higher than that all other bricks (single and double binder).

All the brick specimens except bentonite binder [Reason for failure of bricks with Bentonite as binder has to be explained as bonding due to slag reaction take at elevated temperatures in case of Bentonite] bricks are observed to have the minimum brick compressive strength of 3.5 N/mm² as per the Bureau of Standards (IS: 12894-2002). The AL 1, AC 1, BLC 1 and CLBC 1 bricks met the damp-proof course-2 class brick strength [23, 24] according to (BS 3921:1985).

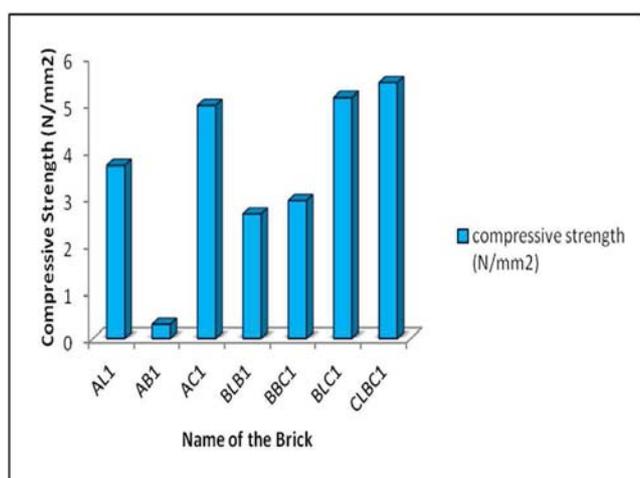


Figure 5. Compressive strength of bricks after 28 days.

4. Conclusion

- (1) Hardening time of the bricks was observed to be 2 days.
- (2) The risk level of toxic metals leaching (Pb, Zn, Ni, Cu, Ni, Co, Cd, and Fe) from the waste materials, after the treatment (S/S) is within the acceptable levels. Therefore the sludge from pharma ETP having a potential to reuse as construction materials for different applications.
- (3) The results of the study showed that the S/S method effectively acceptable for treatment of the hazardous solid waste of the pharmaceutical ETP sludge combined with non-hazardous material (PFA, SF and QD).
- (4) Bentonite alone has been observed to be not suitable as binder in S/S treatment.
- (5) Mixed binders (Cement, Lime, and Bentonite) brick can be recommended for external use in construction i.e. for pave of pedestrian roads. As well as it can be used for furnace constructions.

- (6) This study concludes that the construction raw materials can be replaced with industrial waste by-products in some extended compositions.

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