

Analysis on Influencing Factors of Blasting Vibration Caused by Shallow Tunnel Excavation

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To cite this article:

Haixia Wei, Zheng Qu, Jie Zhu, Qiangqiang Zhang. Analysis on Influencing Factors of Blasting Vibration Caused by Shallow Tunnel Excavation. *American Journal of Civil Engineering*. Vol. 7, No. 4, 2019, pp. 108-112. doi: 10.11648/j.ajce.20190704.14

Received: September 8, 2019; **Accepted:** October 17, 2019; **Published:** October 23, 2019

Abstract: With the widespread construction of urban subway, more and more shallow tunnels will be constructed by blasting, and the problem of blasting vibration will become more prominent. Because of the randomness and variability of blasting source and topographic and geological factors, the propagation mechanism and influencing factors of blasting vibration wave are very complex. Based on blasting-vibration sample data obtained from the established numerical model of blasting excavation in shallow tunnel, the relational degree analysis was carried out for influencing factors of blasting vibration caused by shallow tunnel excavation with method of grey relational analysis. The results of the study are as follows: Among the four related factors, there is no optimal factor, and the maximum charge of one section is the quasi-optimal factor; The charge of the first section is the main factor affecting the peak particle velocity of blasting vibration; The maximum charge of one section is the main factor affecting the main frequency of blasting vibration; The delay interval is the main factor affecting the duration of blasting vibration. Furthermore, the measures to control blasting vibration caused by shallow tunnel excavation were put forward, such as reducing the charge of the first section, reducing the maximum charge of one section and rationally setting up the delay interval. The study has important guiding significance for safe blasting construction in shallow tunnel and scientific control of blasting vibration effect.

Keywords: Shallow Tunnel, Method of Grey Relational Analysis, Blasting Vibration, Influencing Factors, Control Measures

1. Introduction

The subway has been opened in 33 cities in China up to now. In the large-scale development of urban-subway construction, it is inevitable that more and more shallow tunnels will be constructed through the urban areas with many buildings on them. As the most economical and effective excavation method of rock mass engineering, borehole blasting is also the main construction method of rock tunnels. Compared with other blasting projects, the ground surface often has high blasting vibration intensity because of close distance from the blasting source in the blasting construction in shallow tunnels. Blasting vibration caused by underground excavation has become a hot and difficult research topic in the field of blasting engineering in

recent years [1-7]. Because of the randomness and variability of blasting source and topographic and geological factors, the generation and propagation mechanism of blasting vibration wave is very complex. Although a lot of research has been done on the influence factors of blasting vibration and the characteristics of blasting vibration wave [8-13], there are still some problems that have not been fundamentally solved.

Based on blasting-vibration sample data obtained from the established numerical model of blasting excavation in shallow tunnel, the relational degree analysis was carried out for influencing factors of blasting vibration caused by shallow tunnel excavation with method of grey relational analysis. Furthermore, the measures to control blasting vibration caused by shallow tunnel excavation were put forward. The

study has important guiding significance for safe blasting construction in shallow tunnel and scientific control of blasting vibration effect.

2. Principle of Method of Grey Relational Analysis

Method of grey relational analysis is a method to measure the degree of relation among factors according to the similarity or difference of the development trend of factors [14-16]. Method of grey relational analysis has been widely used in industry, agriculture, military, economy, ecology and other fields because of the ability to deal with the grey system with incomplete information, which has relatively high accuracy in the evaluating irregular indicators with small samples.

The specific calculation steps of method of grey relational analysis are as follows [17]:

Step 1: Determine the analysis sequence.

The reference sequence reflecting the behavior characteristics of the system and the comparison sequence affecting the behavior characteristics of the system are determined.

Let the reference sequence $Y = \{Y(k) | k = 1, 2, \dots, n\}$, the comparison sequence $X_i = \{X_i(k) | k = 1, 2, \dots, n\}$, where $i = 1, 2, \dots, m$.

Step 2: Make variables dimensionless.

The data in each factor sequence in the system may be different in dimension, and it is not convenient to compare or it is difficult to get the correct conclusion in comparison. Therefore, the dimensionless processing of data is generally required in the analysis of grey relational degree.

$$x_i(k) = \frac{X_i(k)}{X_i(l)}, k = 1, 2, \dots, n; i = 0, 1, 2, \dots, m \quad (1)$$

Step 3: Calculate the relational coefficient.

The relational coefficient of $x_0(k)$ and $x_i(k)$:

$$\xi_i(k) = \frac{\min_i \min_k |y(k) - x_i(k)| + \rho \max_i \max_k |y(k) - x_i(k)|}{|y(k) - x_i(k)| + \rho \max_i \max_k |y(k) - x_i(k)|} \quad (2)$$

Let $\Delta_i(k) = |y(k) - x_i(k)|$, then

$$\xi_i(k) = \frac{\min_i \min_k \Delta_i(k) + \rho \max_i \max_k \Delta_i(k)}{\Delta_i(k) + \rho \max_i \max_k \Delta_i(k)} \quad (3)$$

where ρ is the resolution coefficient, $\rho \in (0, \infty)$. The smaller ρ is, the greater the resolution is. The general range of ρ is (0, 1). When $\rho \leq 0.5463$, the resolution is the best, usually $\rho = 0.5$.

Step 4: Calculate the relational degree.

Because the relational coefficient is the value of the relational degree between the comparison sequence and the reference sequence at each time, it has more than one number,

and the information is too scattered to make overall comparison conveniently. It is necessary to concentrate the relational coefficient at each time into one value, that is, to find its average value as a quantitative expression of the relational degree between the comparison sequence and the reference sequence.

The formula of r_i is as follows:

$$r_i = \frac{1}{n} \sum_{k=1}^n \xi_i(k), k = 1, 2, \dots, n \quad (4)$$

Step 4: Rank the relational degree.

The relational degree is sorted by size. If $r_1 < r_2$, the reference sequence y is more similar to the comparison sequence x_2 .

After calculating the relational coefficient between sequence $X_i(k)$ and $Y(k)$, the average value of relational coefficients is calculated. The average r_i is called the relational degree between $Y(k)$ and $X_i(k)$.

3. Analysis on Influencing Factors of Blasting Vibration Caused by Shallow Tunnel Excavation

3.1. Determination of System Characteristic Variables and Related Factor Variables

The three main factors of blasting vibration, i.e. particle peak velocity, main frequency and duration, are often taken as the indexes to measure the damage degree of blasting vibration. Because the sample data in this paper are taken from numerical simulation experiments, the average combined velocity and velocity attenuation ratio in a given period of time are selected to represent the duration of blasting vibration in order to shorten the running time of the computer. When analyzing blasting vibration caused by shallow tunnel excavation with method of grey relational analysis, particle peak velocity, main frequency, average combined velocity and velocity attenuation rate were selected as system characteristic variables, and were recorded as Y_1, Y_2, Y_3 and Y_4 respectively.

There are many factors affecting blasting vibration, including total charge, maximum charge of one section, maximum charge in cut section, minimum delay interval, number of sections, distance from blasting centers, number of free surfaces, hole network parameters, geological conditions, etc. The vibration effect produced by cutting blasting in shallow tunnel is the most obvious in practical engineering. Therefore, the excavation process of cutting blasting was simulated by numerical simulation test. Regardless of the factors that can not be quantitatively described, under the condition of constant distance from blasting centers and total charge, the four factors of charge of the first section, maximum charge of one section, number of sections and delay interval were selected as the relevant variables for analysis, which were recorded as X_1, X_2, X_3 and X_4 respectively.

3.2. Acquisition of Sample Data of Blasting Vibration Caused by Shallow Tunnel Excavation

Using numerical software LS-DYNA, the finite element model of cut blasting in shallow tunnel was established, as shown in Figure 1. 3994 is the number of selected surface feature points, from which sample data were obtained. The size of the model is 50m×30m×24m, and the length of the tunnel face without excavation is 24m. Charge diameter is 52 mm, length is 400 mm, mud plugging is 400 mm, single hole charge is 0.85 Kg.

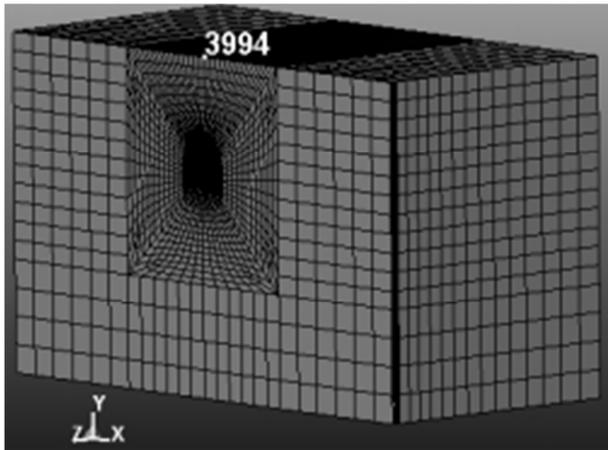


Figure 1. Finite element model of cutting blasting in shallow tunnel.

The explosive material model is defined by JWL state equation:

$$P_{cj} = A(1 - \frac{\omega}{R_1V})e^{-R_1V} + B(1 - \frac{\omega}{R_2V})e^{-R_2V} + \frac{\omega E}{V} \quad (5)$$

where A, B, R_1, R_2, ω are input parameters, $A=371.2\text{Gpa}$, $B=3.231\text{Gpa}$, $R_1=4.15$, $R_2=0.95$, $\omega=0.3$; E is explosive energy, $E=7\text{Gpa}$; TNT is selected as explosive in this model, explosive velocity $v_d=6930\text{m/s}$, density $\rho_0=1630\text{kg/m}^3$, explosion pressure $P_{cj}=0.21\text{Gpa}$.

The blasted rock mass is granite, and the constitutive model of rock mass is isotropic-elastic-plastic material. Its state equation is as follows:

$$p = \frac{\rho_0 c^2 v [1 + (1 - \mu / 2)v - \alpha v^2 / 2]}{[1 - (s_1 - 1)v + s_2 v^2 / (v + 1) - s_3 v^3 / (v + 1)^2]^2} + (\mu + \alpha v)E \quad (6)$$

where $s_1=1.5$, $s_2=0$, $s_3=0$, $\gamma=2.0$, $\alpha=0.5$, $v=1/v_0-1$ (v_0 is relative volume); the material parameters of granite are: Young's modulus $E=66\text{Gpa}$, Poisson's ratio $\mu=0.23$, density $\rho_0=2700\text{kg/m}^3$, wave velocity $c=5268\text{m/s}$, shear modulus $G=23\text{Gpa}$, hardening parameter $n=0.25$.

The mesh arrangement of cut holes is shown in Figure 2. Millisecond blasting of different parameters of charge of the first section, maximum charge of one section, number of sections and delay interval were simulated between 10 boreholes by setting different initiation sequence.

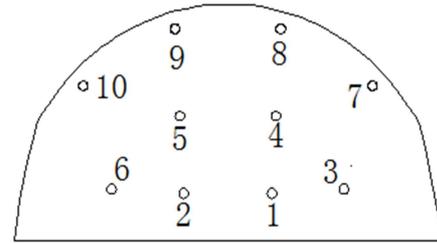


Figure 2. Diagram of mesh arrangement of cutting holes.

Table 1 is a sample of 13 groups of blasting vibration data obtained by using the numerical model to simulate various working conditions.

Table 1. Sample of blasting vibration data.

| No. | Relevant Variables | | | System Characteristic Variables | | | | |
|-----|--------------------|---------------|---------------|---------------------------------|-----------------|---------------|-----------------|--------------|
| | X_1 (kg) | X_2 (kg) | X_3 (ms) | X_4 | Y_1 (cm/s) | Y_2 (Hz) | Y_3 (cm/s) | Y_4 (%) |
| 1 | 5.1 | 5.1 | 35 | 2 | 7.25 | 16 | 0.91 | 87.4 |
| 2 | 3.4 | 3.4 | 35 | 3 | 7.25 | 16 | 0.95 | 86.9 |
| 3 | 6.8 | 6.8 | 35 | 2 | 7.4 | 15.99 | 1.17 | 84.2 |
| 4 | 0.85 | 6.8 | 35 | 3 | 4.05 | 27.99 | 0.77 | 80.9 |
| 5 | 1.7 | 3.4 | 35 | 3 | 5.26 | 83.96 | 0.86 | 83.7 |
| 6 | 1.7 | 6.8 | 35 | 2 | 4.89 | 31.98 | 0.76 | 84.5 |
| 7 | 1.7 | 3.4 | 35 | 4 | 4.89 | 31.98 | 0.84 | 82.8 |
| 8 | 5.1 | 5.1 | 0 | 2 | 13.0 | 62.83 | 1.51 | 88 |
| 9 | 5.1 | 5.1 | 8 | 2 | 8.36 | 10.95 | 1.21 | 85 |
| 10 | 5.1 | 5.1 | 15 | 2 | 9.66 | 91.95 | 0.99 | 0.99 |
| 11 | 5.1 | 5.1 | 35 | 2 | 6.67 | 91.95 | 1.07 | 1.07 |
| 12 | 5.1 | 5.1 | 50 | 2 | 6.67 | 59.97 | 1.14 | 1.14 |
| 13 | 5.1 | 5.1 | 70 | 2 | 6.67 | 63.97 | 1.09 | 1.09 |

3.3. Calculation of Grey Relational Degree

In order to determine the positive and negative relation between the related variables and the system characteristic variables, the relation should be transformed by axial symmetry method. Explosion charge is negatively related with main frequency, number of sections and delay interval is negatively related with particle peak velocity, the relevant variables are positively related with average combined velocity and velocity attenuation rate. Initial data are usually transformed into dimensionless data with similar order of magnitude in the process of grey relational analysis, and the negative relation factors are transformed into positive relation factors. Based on the sample data in Table 1, the grey relational matrix of the factors affecting blasting vibration was calculated with method of grey relational analysis, as shown in Table 2.

Table 2. Grey relational matrix of the factors affecting blasting vibration.

| Relational Degree | X_1 | X_2 | X_3 | X_4 |
|-------------------|--------|--------|--------|--------|
| Y_1 | 0.7792 | 0.7619 | 0.7252 | 0.6878 |
| Y_2 | 0.6857 | 0.7337 | 0.6057 | 0.5928 |
| Y_3 | 0.7039 | 0.7410 | 0.8493 | 0.7432 |
| Y_4 | 0.7281 | 0.7559 | 0.7563 | 0.6605 |
| Σ | 2.8969 | 2.9925 | 2.9365 | 2.6843 |

3.4. Analysis on Influencing Factors of Blasting Vibration Caused by Shallow Tunnel Excavation

Referring to the grey relational matrix of the influencing factors of blasting vibration in Table 2, superiority ranks analysis of the related variables were carried out, and the following conclusions can be drawn:

The superiority ranks of influencing factors of blasting vibration caused by shallow tunnel excavation in the order of high to low are: maximum charge of one section, charge of the first section, delay interval and number of sections; there is no optimal factor, and the maximum charge of one section is the quasi-optimal factor.

The superiority ranks of influencing factors of particle peak velocity for blasting vibration in the order of high to low are: charge of the first section, maximum charge of one section, delay interval and number of sections; combining with the comparative analysis of particle peak velocity of different charge of the first section in Table 1, it is shown that the charge of the first section is the main factor affecting the peak velocity of blasting vibration.

The superiority ranks of influencing factors of main frequency for blasting vibration in the order of high to low are: maximum charge of one section, charge of the first section, delay interval and number of sections; the maximum charge of one section is the main factor affecting the main frequency of blasting vibration.

The superiority ranks of influencing factors of average combined velocity and velocity attenuation rate for blasting vibration in the order of high to low are: delay interval, maximum charge of one section, charge of the first section and number of sections; delay interval is the optimal factor for the two system characteristic variables, which is also the main factor affecting the duration of blasting vibration. In the superiority ranks of the factors affecting the duration, the ranks of the factors affecting the average combined velocity and the velocity attenuation ratio show consistency, which indicates that the two parameters selected to represent the duration of blasting vibration are reasonable.

As one of the influencing factors of blasting vibration, the number of sections is not a quasi-optimal factor and the main influencing factor. Excessive increase of the number of initiation sections is not an effective means to control the blasting vibration effect in millisecond blasting.

4. Control Measures of Blasting Vibration Caused by Shallow Tunnel Excavation

Based on the above conclusions, the following measures are suggested to control the blasting vibration caused by shallow tunnel excavation:

To reduce the charge of the first section. Because the number of free surfaces is small and the initiation energy of the first section is too concentrated, the blasting vibration caused is large. At the same time, due to the serious shortage

of compensation space after blasting, blasting rock is subject to greater resistance when it disperses, and the blasting effect is poor. Therefore, reducing the charge of the first section can effectively control the blasting vibration intensity and improve the blasting effect.

To reduce the maximum charge of one section. The maximum charge of one section is the main factor affecting blasting vibration. Therefore, under the condition of constant total blasting charge, the blasting vibration intensity can be effectively reduced by properly increasing the initiation sections and reducing the maximum charge of one section.

To set up rational delay interval. For millisecond blasting of shallow tunnel, reasonable delay interval is more effective than increasing the number of sections. Cutting holes can be set as jump-off, which can prolong the interval between sections properly and prevent the superposition of blasting seismic waves, so as to achieve the purpose of vibration reduction. Cutting holes can be set as jump-off blasting holes, which can prolong the interval between sections and prevent the superposition of blasting vibration waves, so as to achieve the purpose of vibration reduction.

5. Conclusion

The sample data of blasting vibration were obtained by establishing finite element model of cut blasting in shallow tunnel. Based on the sample data, the relational degree analysis was carried out for influencing factors of blasting vibration caused by shallow tunnel excavation with method of grey relational analysis. The analysis results show that: among the four relevant influencing factors, there is no optimal factor, and the maximum charge of one section is the quasi-optimal factor; the charge of the first section is the main factor affecting the peak velocity of blasting vibration; the maximum charge of one section is the main factor affecting the main frequency of blasting vibration; the delay interval the main factor affecting the duration of blasting vibration.

Based on the conclusion of grey relational analysis, the measures to control blasting vibration caused by shallow tunnel excavation were put forward, such as reducing the charge of the first section, reducing the maximum charge of one section and rationally setting up the delay interval.

There are many factors affecting blasting vibration caused by shallow tunnel construction. Only some of the factors were considered based on the numerical test model in this paper. It is suggested that field tests can be carried out to further analyze the influence of other factors such as number of free surfaces, hole network parameters and geological conditions.

Acknowledgements

The authors would like to acknowledge the financial support from the National Natural Science Foundation of China (51504082 and 51874123) and the Science and Technology Research Planning Project of Henan Province, China (152102310331).

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