
Experimental Analysis of Seepage in Soil Beneath a Model of a Gravity Dam

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Abstract: In this research the experimental method by using Hydraulic modeling used to determination the flow net in order to analyses seepage flow through single- layer soil foundation underneath hydraulic structure. As well as steady the consequence of the cut-off inclination angle on exit gradient, factor of safety, uplift pressure and quantity of seepage by using seepage tank were designed in the laboratory with proper dimensions with two cutoffs. The physical model (seepage tank) was designed in two downstream cutoff angles, which are (90, and 120°) and upstream cutoff angles (90, 45, 120°). After steady state flow the flow line is constructed by dye injection in the soil from the upstream side in front view of the seepage tank, and the equipotential line can be constructed by piezometer fixed to measure the total head. From the result It is concluded that using downstream cut-off inclined towards the downstream side with Θ equal 120° that given value of redaction (25%) is beneficial in increasing the safety factor against the piping phenomenon. Using upstream cut-off inclined towards the downstream side with Θ equal 45° that given value of redaction (52%) is beneficial in decreasing uplift pressure and quantity of seepage.

Keywords: Flow Net, Inclined Cutoff, Seepage Tank, Single Layer, Soil

1. Introduction

Hydraulic structures are a specific type of engineering structures designed and executed in such a way in order to control natural water or save industrial sources to guarantee optimum use of water. These structures are frequently build on soil materials and the foundation thickness must be thick so as to be safe against uplift pressure [1]. The differential head in water levels between the upstream and downstream acts on the foundation and causes seepage flow [2]. The Groundwater flow depends on the type of flow, the soil media, and the boundary conditions. Seepage of water is one of the main problems which effect on hydraulic structures [3]. There are Different methods solution can be used to analysis the seepage problem such as experimental works using physical model as well as numerical models electrical analog models[4]. A flow net is in fact a solution of Laplace's equation in two dimensions. The model of seepage tank (sand tank)is very useful in studying the conditions of fluid flow under the hydraulic structure [5]. The paths taken by moving particles of water as the flow through a permeable material

may be represented by a series of flow lines. These flow lines are nearly parallel curved lines The hydraulic modeling method to determine the flow net in this study represented by a physical model was built to study the phenomenon of seepage through soil.

2. Aim of the Study

The main objectives of this work can be summarized by the following points:

1. locate the equipotential lines and flow lines for single-layer soil used in research work.
2. Study the effect of inclined cutoffs at different angles of inclination on exit gradient, uplift pressure underneath the hydraulic structure quantity of seepage and find the best inclination angle of cut-off for upstream and downstream side of hydraulic structure for all types of soils placed in different position under the foundation of hydraulic structure used in research work.

3. Experimental Work

The results obtained by the present hydraulic model using the seepage tank that designed and carried out at the hydraulic laboratory of the Engineering College at Babylon University. The major purpose of the physical model adopted in the present research is to study the flow net and calculate the values of uplift pressure underneath the hydraulic structure, distribution of exit gradient, quantity of seepage for different types of soil at different position under the hydraulic structure foundation.

3.1. Model Description

Laboratory experiments have been conducted in a seepage

tank that has been designed with hypothetical dimensions of 1.6 m long, 0.5m width and 1.1m height. The bottom and sidewalls of this tank were made of Acrylic of (10mm) thickness. Figure (1) shows the seepage tank used in present study (front view). The bottom of the tank was filled with this material of soil to a depth of 60 cm. Acrylic walls were used to build the body of the superstructure which consists of two parts. The first part simulated as foundation of a structure (40 cm long × 50 cm wide). This base is connected with the upstream and downstream cutoffs by gluing rubber strips. 10 piezometers were placed at the right side of the tank at different location. All piezometers are fixing to the board.

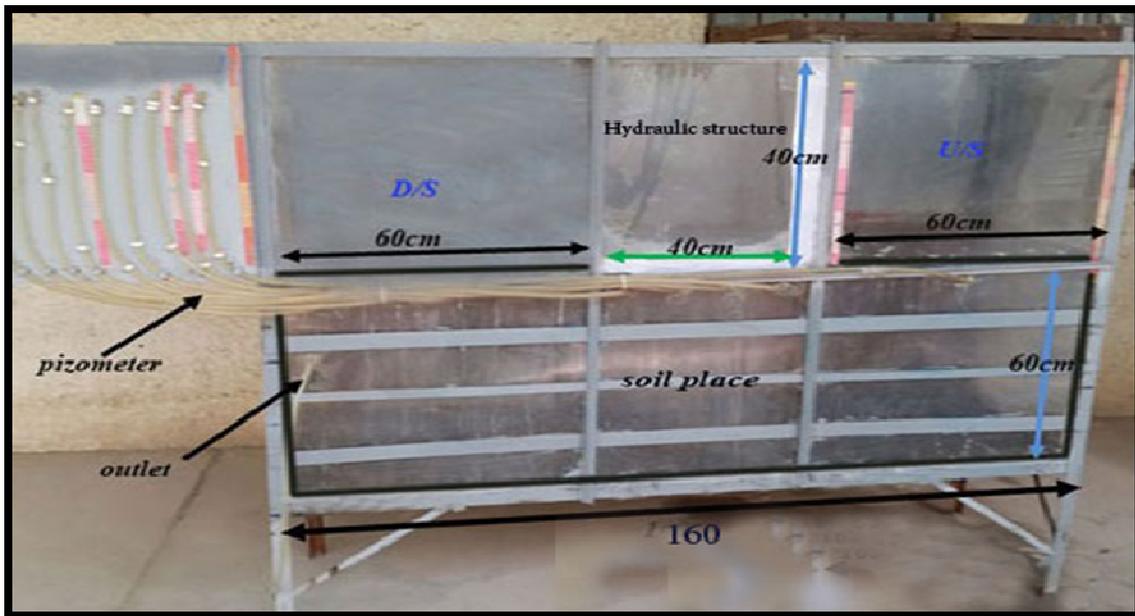


Figure (1). The seepage tank used in present study (front view).

3.2. Engineering Properties of Soil Used in Research

The experimental soil sample was taken from Hilla city region. The soil profile of any region contains many soil horizons, the difference between these horizons is marginal (no-homogenous soil). In the model tests, the profile is assumed to consist of one horizon (homogenous soil) [6]. The tests used here to analyze the soil specimen in order to determine soil distribution and other engineering properties

were conducted as per the Unified Soil Classification System, also the hydraulic conductivity values of the soil samples was measured in laboratory method. Table 1 shows a summary of the physical properties that measured of the soils which consist of three layers arranged in descending order. Used in the present study. Figure (1) shown the arranged for type of soil used in present study.

Table (1). Physical properties of used soils.

| No of layer. | Type off soil Arrange in descending order | Void ratio | Unit weight KN/m ³ | Gs | Value of Hydraulic Conductivity m/sec |
|--------------|---|------------|-------------------------------|------|---------------------------------------|
| 1 | Sandy silty clay | 0.52 | 20.65 | 2.75 | 5.23*10 ⁻⁷ |

3.3. The Experimental Procedures

Taking the datum to be at the bottom of the tank, Install the soil in the form of three layers each layer thickness of 0.2m and it is monitoring the process of using. The metal cylinder.

Feeding the water to the seepage tank through the inlet hose until the water level in the upstream region reached the overflow hose level previously adjusted to meet the desired upstream water level.

After reaching steady-state flow dye is injected from dye

bottles which placed in the specific points , after a period of time flow lines were drawn Flux, which represents how the flow of water within the soil particles

After drawing flow lines, the vertical piezometers were installed transparent glass vertically into the soil to measure the total head in the points to draw the equipotential line.

Measure the discharge of drained water collected from the downstream funnel using the volumetric method by using jar.

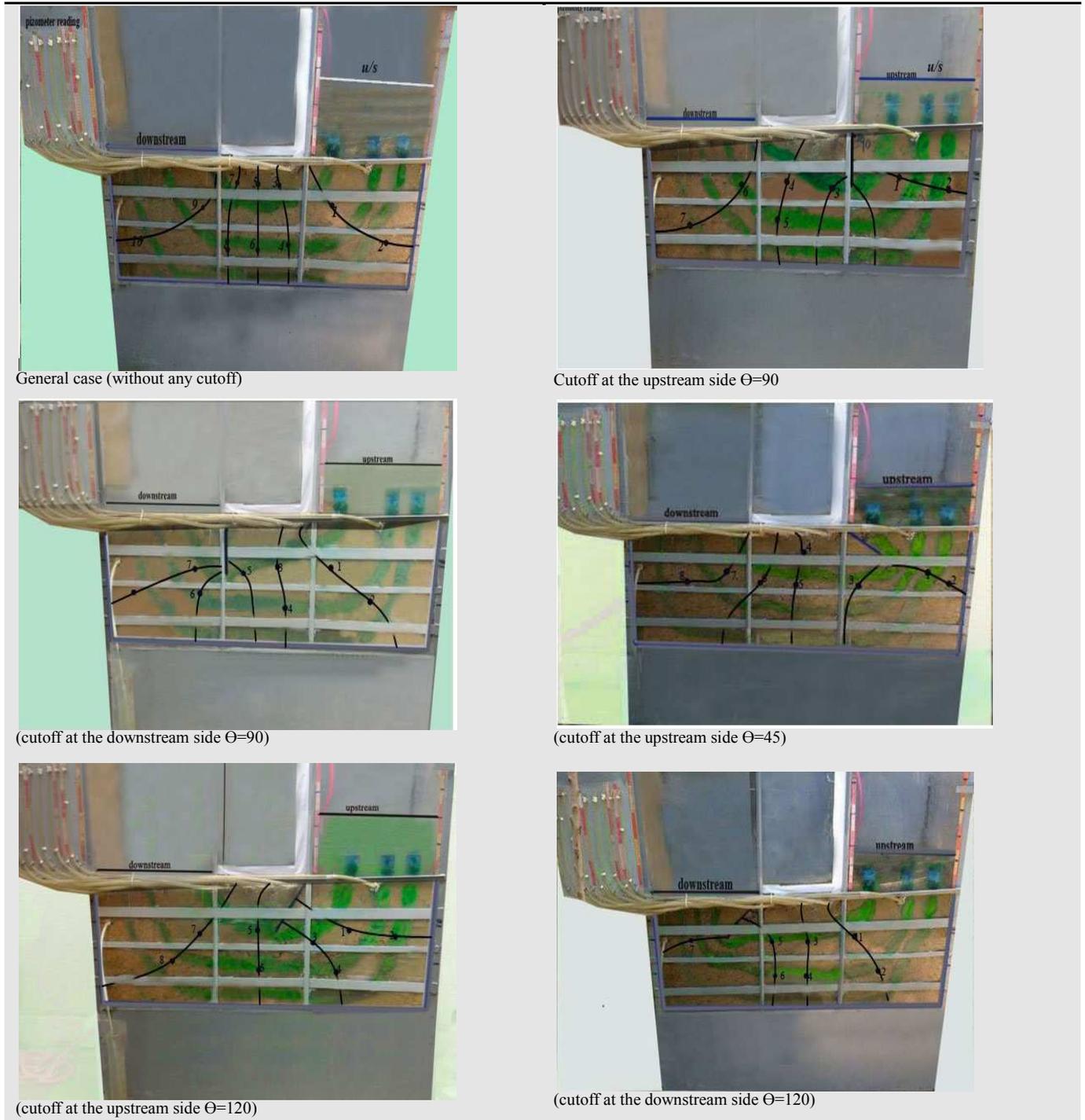
Record the reading of the piezometric head of all installed piezometers under the base and downstream side.

Put the cutoff at upstream side with the angle of inclination for upstream($\Theta=45$, $\Theta=120$, $\Theta=90$) and repeat the step (7-8-9) to find the best angle that gave less value of uplift pressure and quantity of seepage.

Put the cutoff at downstream side with the angle of inclination ($\Theta=90$, $\Theta=120$) and repeat the step (7-8-9) to find the best angle to give max value factor of safety.

Table (2) shown the type of testing that made on multi layer soil

Table (2). The type of testing that made on soil.



4. The Results and Discussions

Herein, the discussions of the results for single layer (sandy silty clay) according the following parameters:

4.1. Effect of Inclination Cutoff and its Position on the Uplift Head

As shown in figure (2). When the Cutoff in upstream side of hydraulic structure was inclination with different angles, its noticed that the uplift pressure underneath the hydraulic structure decreases as(Θ) decreases toward U/S side for Θ (45° , 90° , 120°) where the maximum redaction in uplift pressure according to the general case $\Theta=0$ (without any cutoff) was (57% , 45% ,22%) respectively so that the best angle is 45° .

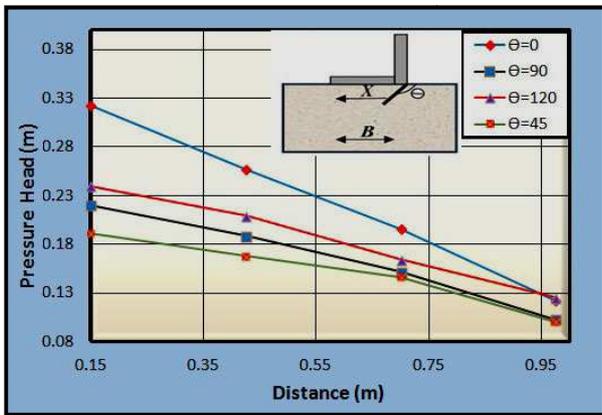


Figure (2). Uplift head ratio through foundation . A range of (Θ) values for cutoff in U/S.

From figure (3). When the Cutoff in downstream side of hydraulic structure is used, the uplift pressure obtained decreases as (Θ) decreases toward U/S side for Θ (90° and 120°) and the maximum redaction in uplift pressure according to the general case $\Theta=0$ was (2.3% ,and2.74%). It is noticed that the redaction of the uplift pressure is small to the replacing of the cut-off ,therefore, it is not suggested at any angle of inclination.

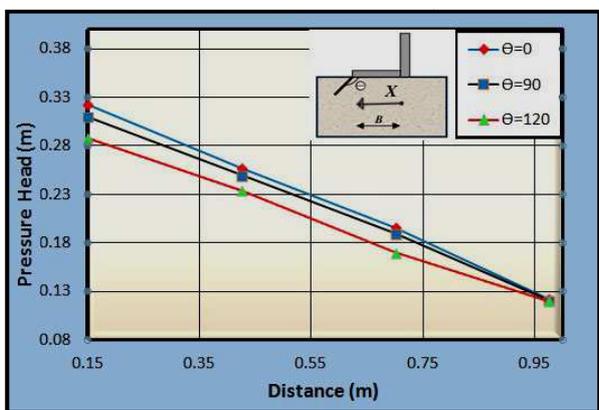


Figure (3). the value of uplift head for different values of (Θ) values for cutoff in D/S part of structure.

When the cutoff positioned in U/S and D/S part of structure as shown figure(4), the uplift reduced strongly and value of redaction is 38% as compared with general case ($\Theta=0$) .

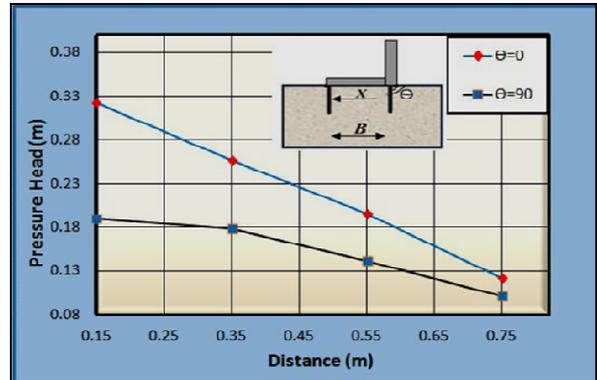


Figure (4). Uplift head ratio through foundation a range of (Θ) values for cutoff in U/S and D/S.

4.2. Effect of inclination Cutoff and its Position on the Exit Gradient

The exit gradient was studied at the end of the hydraulic structure for the cases that will be discussed herein and the results are represented graphically. The factor of safety for each angle of inclination must be calculated where is equal to the division of exit gradient on critical gradient (I_{cr}) which is dependent on the specific gravity (G_s) and void ratio (e) of the soil particles [$I_{cr} = (G_s-1)/(1+e)$]. In this study and for this type of soil ($G_s = 2.75$, $e = 0.77$, $I_{cr} = 0.988$).

In figure(5) when the cutoff put in upstream side of hydraulic structure it is found that the redaction in values of exit gradient were so small and as follows for $\Theta(45^\circ, 90^\circ, 120^\circ)$ where the maximum redaction in according to the general case $\Theta=0$ (without any cutoff) was (1.2% , 1.87% ,2.47%) respectively

The result shows that the upstream cut-off inclination angle has no noticed effect on exit gradient. From the result the factor of safety against piping for this case were shown in table (3).

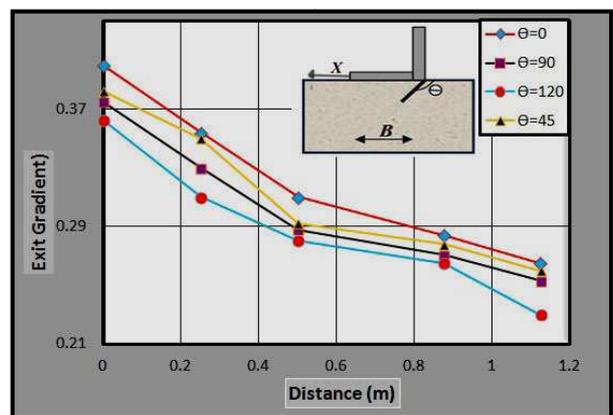


Figure (5). Exit gradient a range of (Θ) values for cutoff in U/S part of structure.

Table (3). The factor of safety against piping when cutoff at U/S.

| U/S Cut-off Inclination | Max (exist gradient) | Fs |
|-------------------------|----------------------|-------|
| 0° | 0.4 | 2.47 |
| 45° | 0.382 | 2.586 |
| 90° | 0.375 | 2.63 |
| 120° | 0.362 | 2.729 |

In figure(6) when the cutoff is put it in downstream side of hydraulic structure the exit gradient decreases as (Θ) increases toward the D/S side for Θ (90° and 120°) the maximum redaction in exist gradient according to the general case $\Theta=0$ was (12.5% and 25%), respectively . So that the factor of safety against piping phenomenon of this case can be calculated as shown in table (4).These results show that using cutoff in D/S side inclination toward D/S $\Theta=120$ increasing the factor of safety against piping.

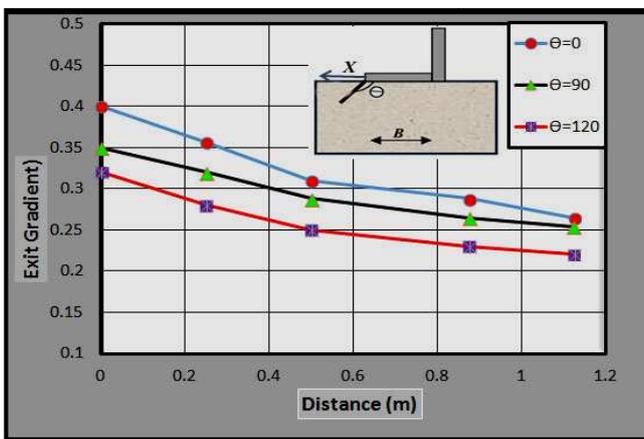


Figure (6). Exit gradient a range of (Θ) values for cutoff in U/S part of structure.

Table (4). The factor of safety against piping when cutoff at U/S.

| U/S Cut-off Inclination | Max (exist gradient) | Fs |
|-------------------------|----------------------|------|
| 0° | 0.4 | 2.47 |
| 90° | 0.35 | 2.82 |
| 120° | 0.31 | 3.18 |

When the Cutoff in up and down stream side of structure the exit gradient in the bed level of structure decreases compare with general case as shown in figure (7).

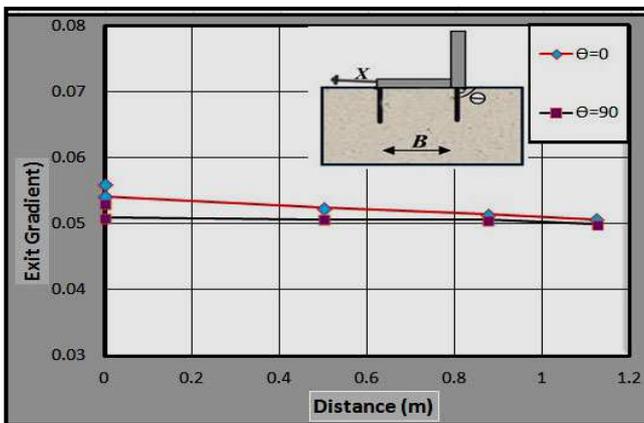


Figure (7). Exit gradient a range of (Θ) values for cutoff in U/S part of structure.

4.3. Effect of Cutoff Position and Inclination on the Seepage Quantity

When the Cutoff is in upstream side of hydraulic structure, as shown in figure(8), it's found that the seepage decreases while (Θ) decrease toward U/S , and the least quantity of seepage occurred when (Θ) value around (45).

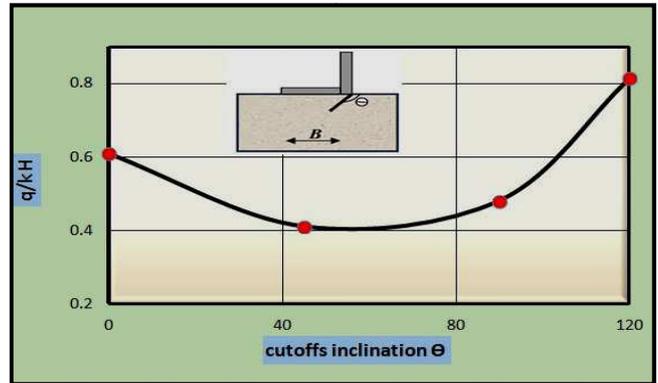


Figure (8). The Seepage quantity a range of different values (Θ) for cutoff in U/S part of structure.

In figure(9) When the Cutoff is in upstream side of hydraulic structure the seepage decreases while (Θ) increases, and the least quantity of seepage occurred when (Θ) value around (120), then the seepage increases rapidly for $(\Theta \le 90)$.

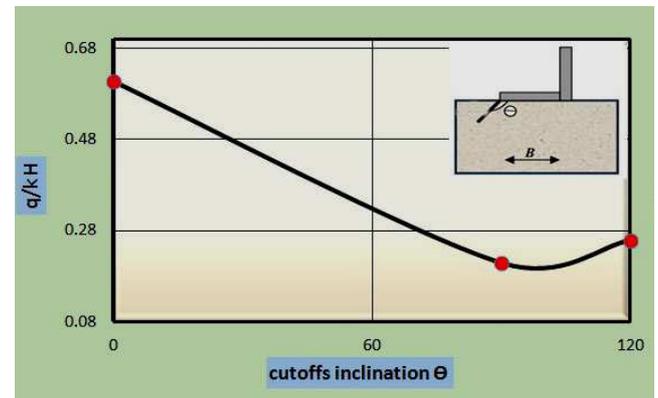


Figure (9). The Seepage quantity a range of different values (Θ) for cutoff in D/S part of structure.

5. Conclusions

The following main conclusions can be drawn from the results presented in this research:

The shapes of the flow net depend upon many factors such as diameter of the particle of the soil and location of cutoff.

The minimum value of uplift pressure is obtained when the cutoff used in upstream part of hydraulic structure with angle of inclination $(\Theta = 45^\circ)$. That given redaction in value of uplift pressure according to the general case $\Theta=0$ was 53%.

The minimum value of exist gradient is obtained when the cutoff used in downstream part of hydraulic structure with angle of inclination $(\Theta = 120^\circ)$ That given redaction in value of exist gradient according to the general case $\Theta=0$ was 9.3%.

And increasing the factor of safety against piping to 2.06.

Placing the cutoff at the dam heel (cutoff U/S side) to reduce the piping phenomenon in downstream side is not recommended under any angle of inclination, because such placement has too small effect.

The best angle of inclination is 45° towards upstream where it reduced the uplift pressure to (43% according to general case $\Theta=0$) as compared with other type of inclination and reducing the quantity of seepage.

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